

APPENDIX D

PUMP TECHNICAL INFORMATION



September 21, 2007

Cathy Busking
Busking Engineering
627 S. Euclid Avenue
Oak Park, IL 60304

MPC No. BQ-27151

**RE: MORRISON BUDGET QUOTE NO. 27151
MWRDGC Effluent Pumps**

Dear Cathy,

Morrison Pump Company is pleased to provide this Budget Quotation for Pump Equipment for the MWRDGC Effluent Pumping Project, as per our pump selection emailed to you on September 11, 2007. Pumps are per typical municipal, final effluent pump specifications, and per Hydraulic Institute Standards. Specifications are attached.

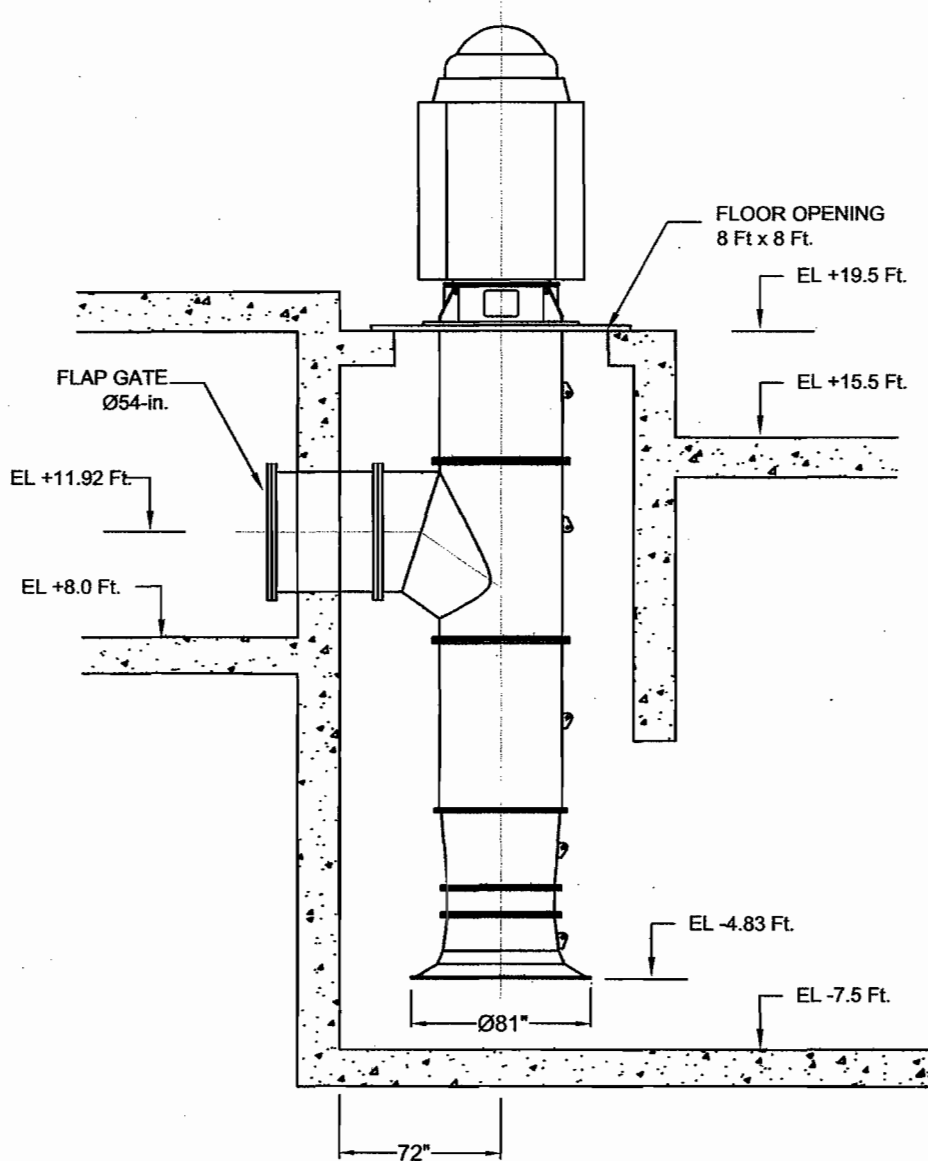
<u>Equipment</u>	<u>Total Budget Price</u>
Six (6) Morrison Vertical Pumps Model VPS-54-47-02, with 250 HP @ 325 RPM Vertical Electric Motor Drivers, Motor Control Center with VFDs, each pump providing 78,000 GPM @ 7.5 Ft. TDH	\$ 3,500,000.--

Pricing is to be understood net, delivered to site, without applicable taxes. Included with our equipment are complete technical submittals, factory performance testing, delivery to site, field services for installation & start-up, and one year standard warranty.

Sincerely,

Jorge M. Cortes

GENERAL PUMP LAYOUT



NOTES:

- LAYOUT IS FOR GENERAL REFERENCE ONLY.
- FLOOR OPENING REQUIREMENT = 96" x 96" SQUARE; PUMP BASEPLATE = 116" x 116"
- PUMP DISCHARGE = Ø54-INCHES.
- PUMP SUCITON BELL = Ø81-INCHES.
- ELECTRIC MOTOR = TEFC, VSS, 250 HP @ 325 RPM, 460V/3PH/60HZ



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THE INFORMATION PROVIDED IS
PROPRIETARY AND FOR GENERAL
REFERENCE ONLY.

DWG. TITLE:

Morrison Pump Model VPS-54-47-02 - Station Layout

FILE NAME:

MWRGC North Side Water Reclamation Plant - CTE Engineering

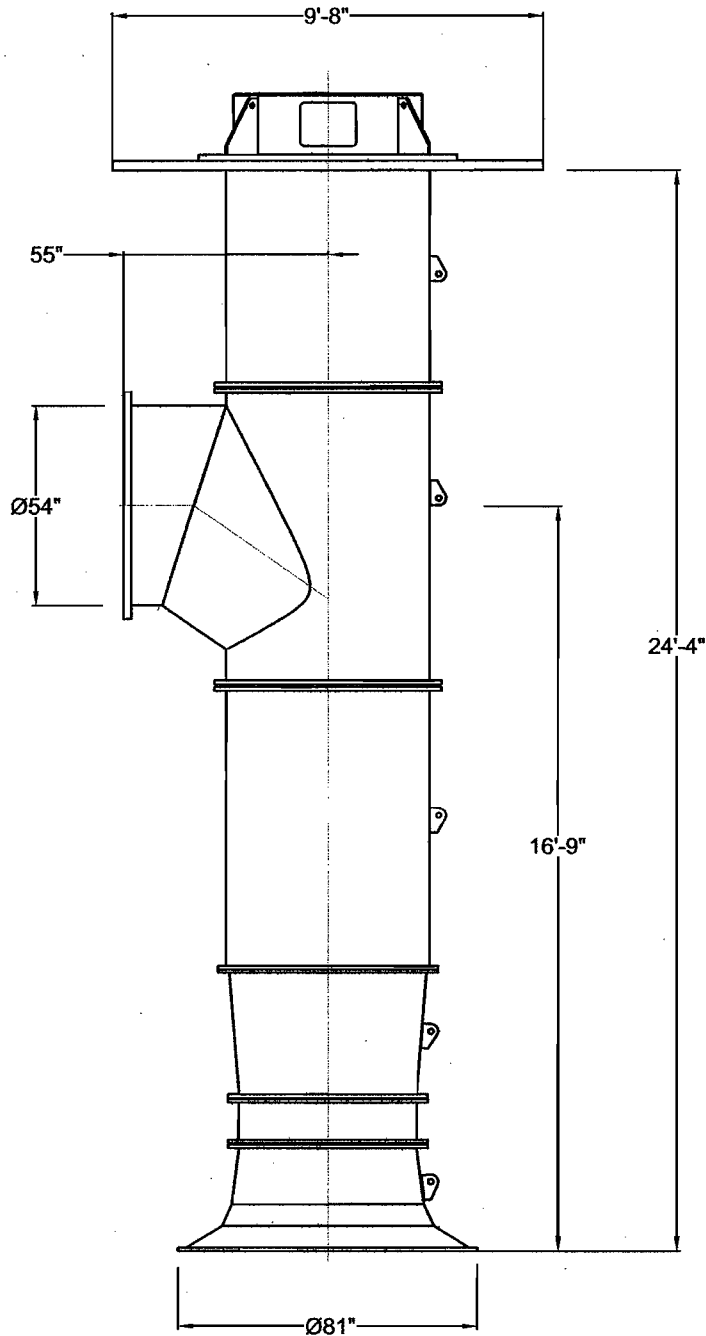
DWG NO.:

DWG-27151-002

DATE:


11-SEPT-2007

GENERAL PUMP DIMENSIONS



NOTES:

- DIMENSIONS ARE FOR GENERAL REFERENCE ONLY.
- ESTIMATED PUMP WEIGHT = 20,000 LBS.
- PUMP INCLUDES REMOVABLE (SPLIT) BASEPLATE, 116" X 116" SQUARE


MORRISON
PUMP COMPANY

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DWG. TITLE:
Morrison Pump Model VPS-54-47 General Dimensions

FILE NAME:
MWRGC North Side Water Reclamation Plant - CTE Engineering

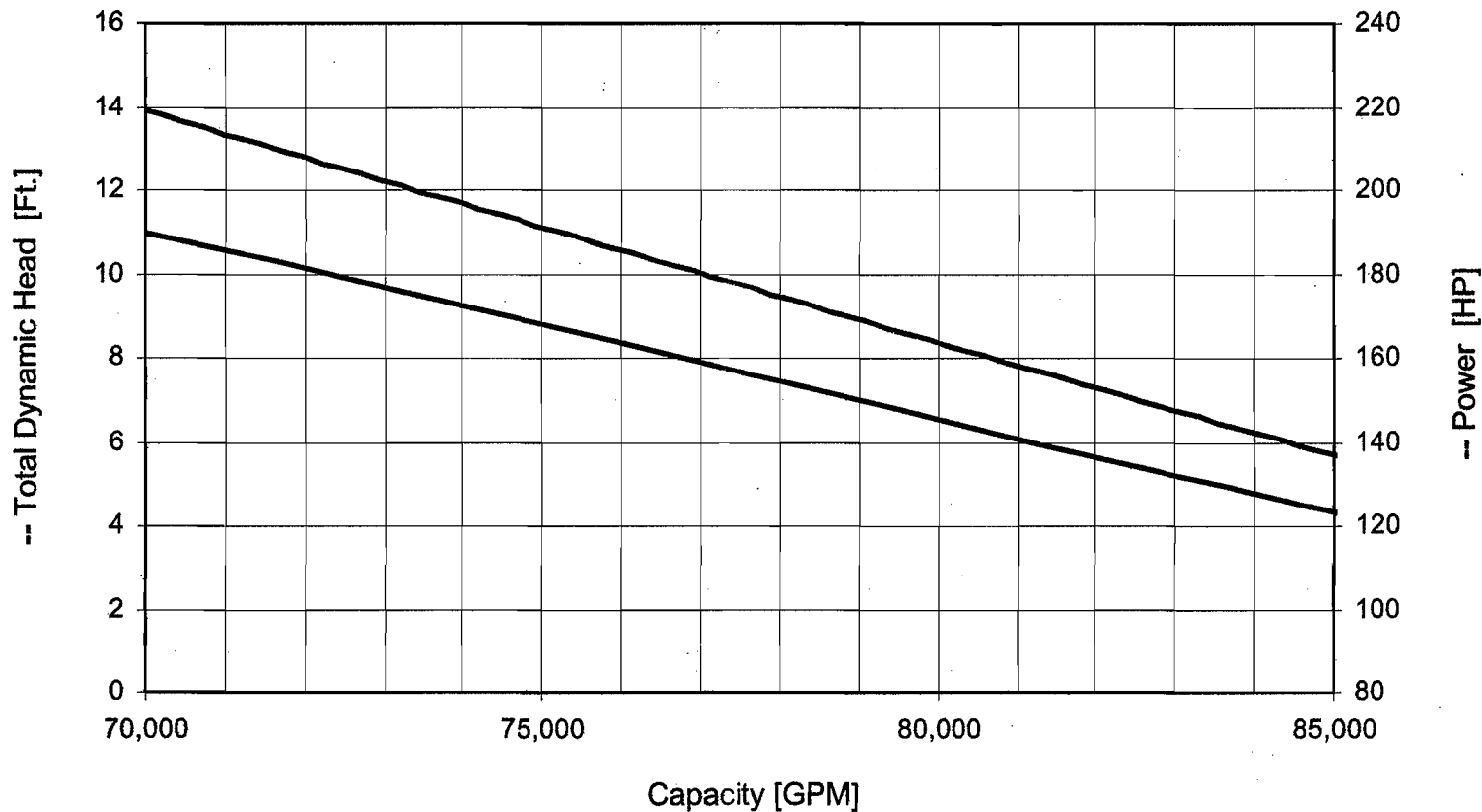
DWG NO.:
DWG-27151-001

DATE:
11-SEPT-2007

Pump Performance

Axial Flow Impeller, Single Stage, High-Efficiency

Project No.: 27151
Project Name: MWRDGC North Side Water Reclamation Plant – CTE Engineering
Date: 11-September-2007



Pump Bowl Model No.: 47-02-CH
Impeller Diameter: 46.9 in. (1190 mm.)
Shaft Speed: 325 RPM

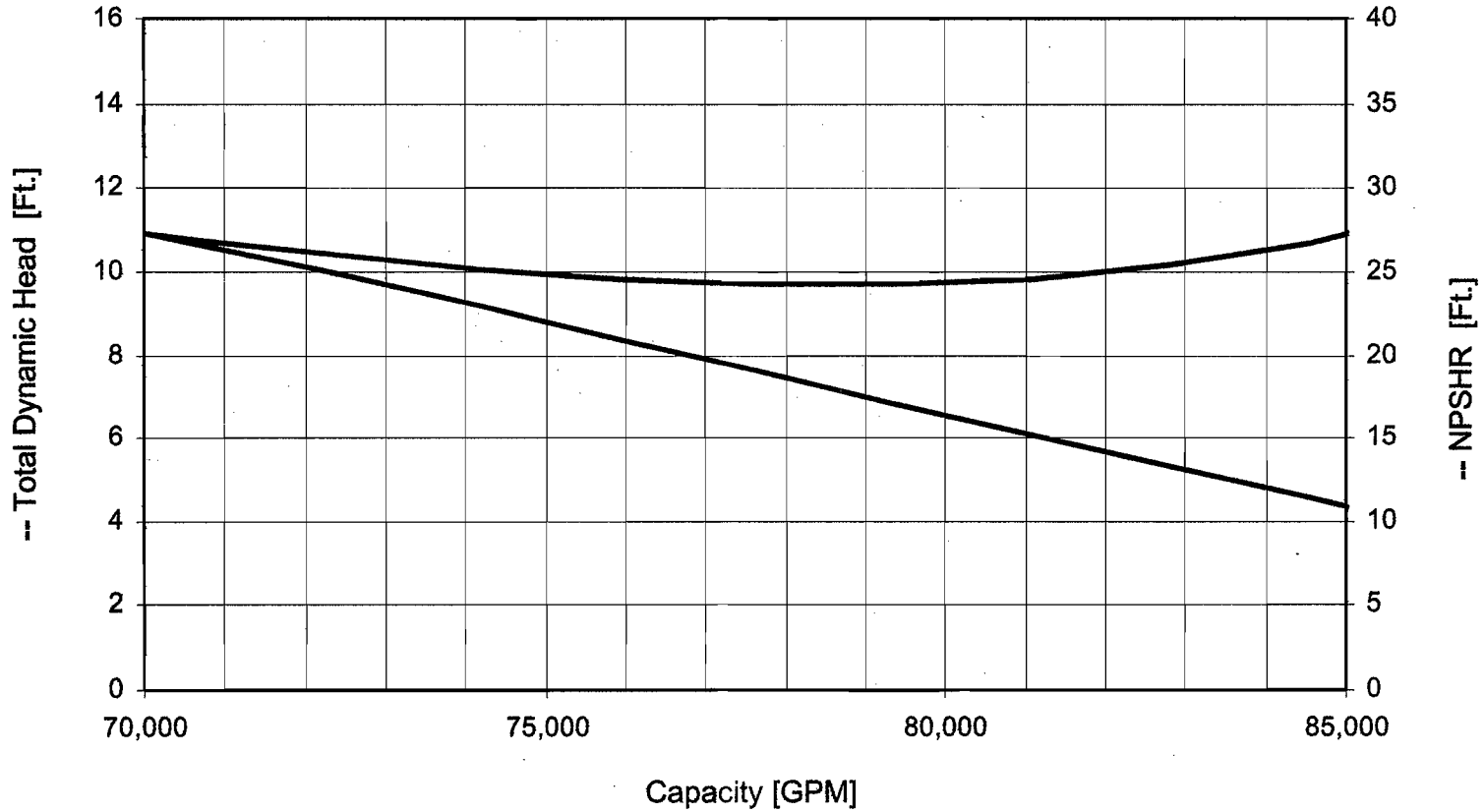


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The curve provided is proprietary and for general reference use only. Please consult factory for specific pump operating characteristics and certified performance curves.

Pump Performance

Axial Flow Impeller, Single Stage, High-Efficiency

Project No.: 27151
Project Name: MWRDGC North Side Water Reclamation Plant – CTE Engineering
Date: 11-September-2007



Pump Bowl Model No.: 47-02-CH
Impeller Diameter: 46.9 in. (1190 mm.)
Shaft Speed: 325 RPM

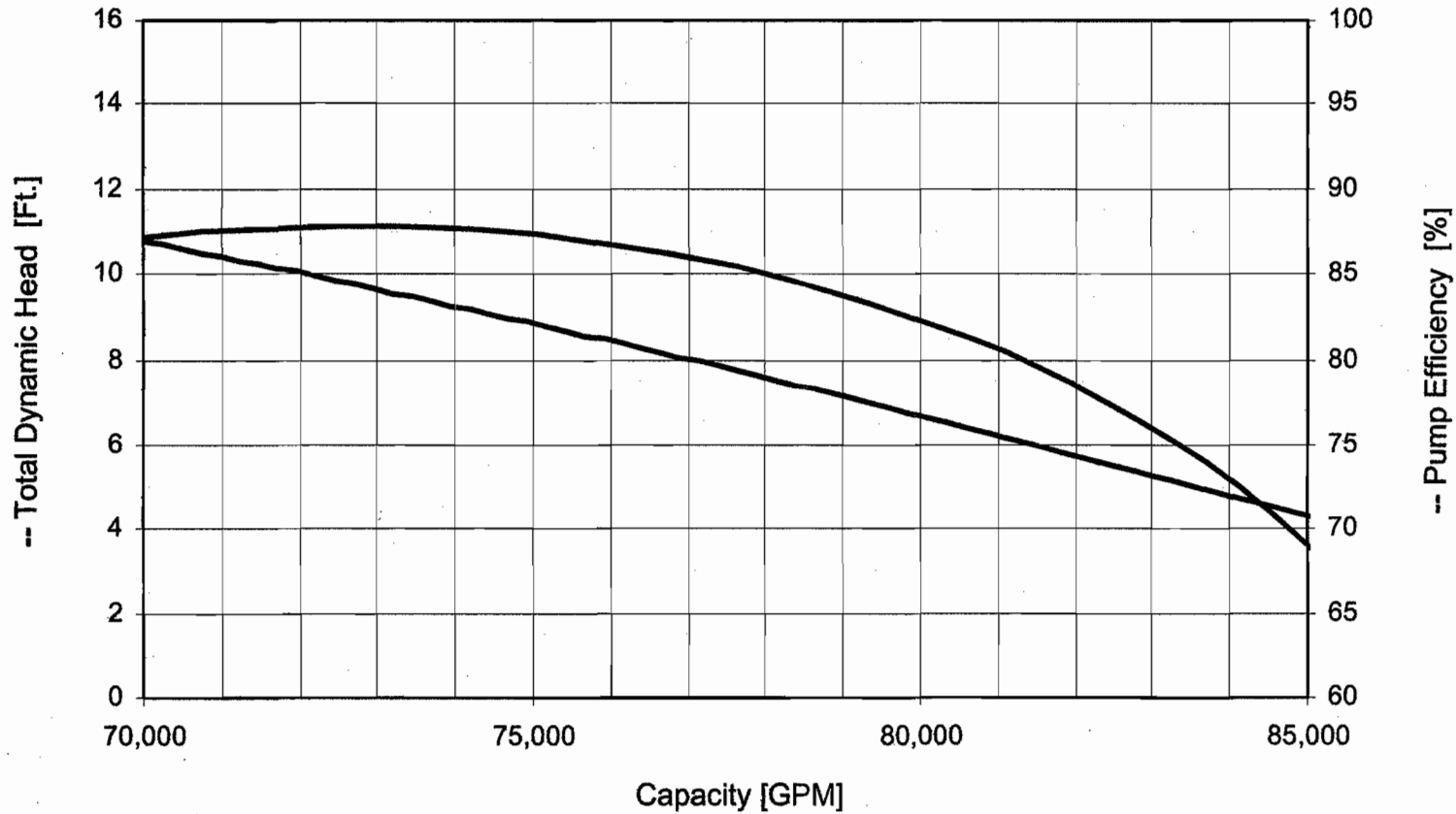


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characteristics and certified performance curves.

Pump Performance

Axial Flow Impeller, Single Stage, High-Efficiency

Project No.: 27151
Project Name: MWRDGC North Side Water Reclamation Plant – CTE Engineering
Date: 11-September-2007



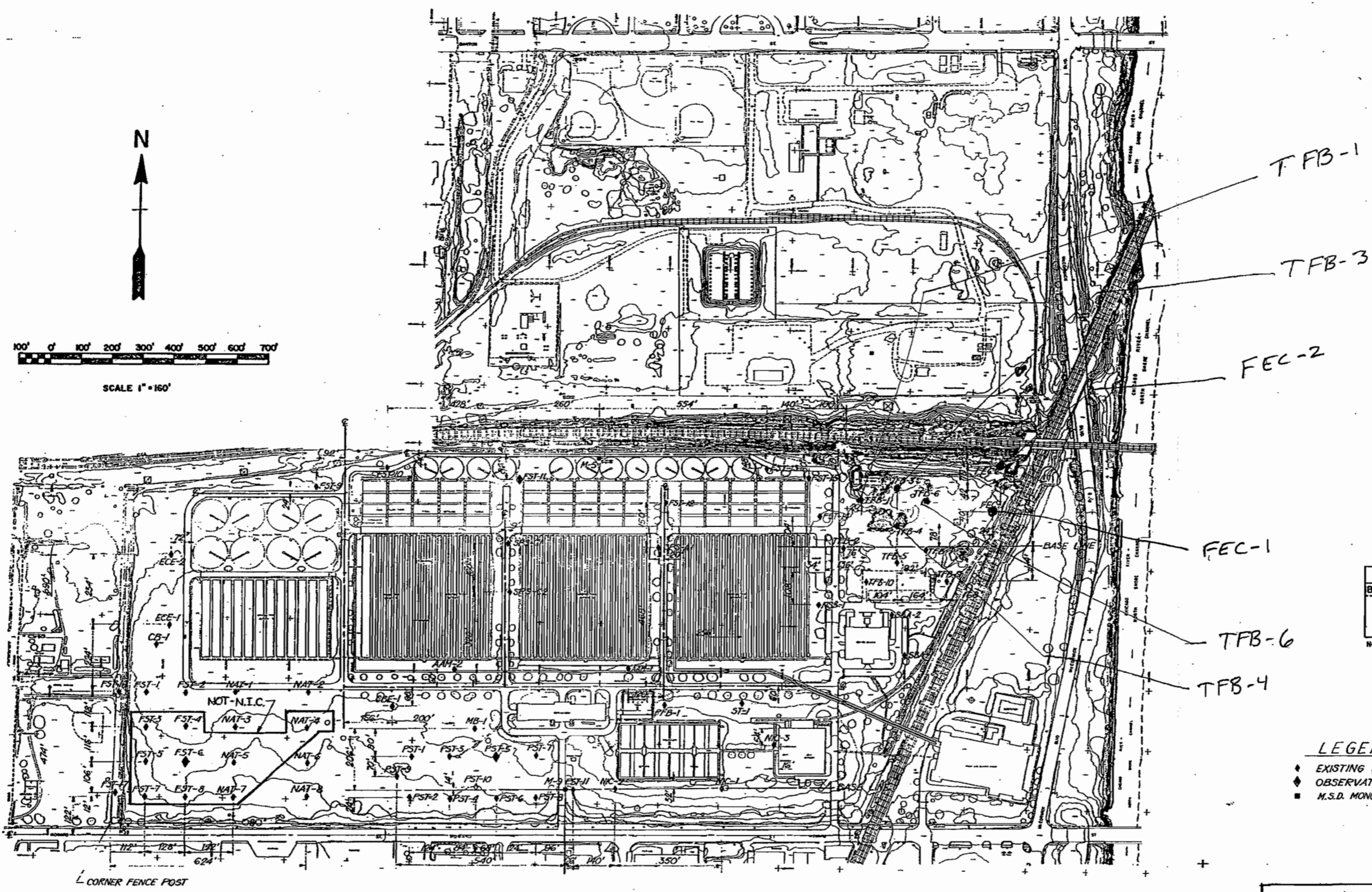
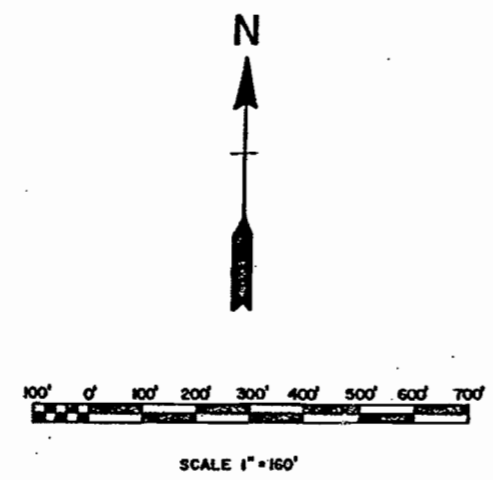
Pump Bowl Model No.: 47-02-CH
Impeller Diameter: 46.9 in. (1190 mm.)
Shaft Speed: 325 RPM



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characteristics and certified performance curves.

APPENDIX E

HISTORICAL SOIL BORING INFORMATION



OBSERVATION WELLS	
BORING NO.	ELEV. OF € BRASS TIP
FST-11	- 900 C.C.D.
FST-5	- 1250 C.C.D.
FST-6	- 925 C.C.D.
TFB-4	- 1250 C.C.D.

NOTE: € of Brass Tip 6.5' Below Elevation of Deepest Foundation.

LEGEND

- ◆ EXISTING BOREHOLES
- ◆ OBSERVATION WELLS
- M.S.D. MONUMENT

NOTE - N.I.C. FUTURE WORK NOT IN THIS CONTRACT

RETA ENGINEERS / A JOINT VENTURE
CHICAGO

REVISIONS		
NO.	DATE	BY
Δ	5/1/84	MSDGC

**THE METROPOLITAN SANITARY DISTRICT
OF GREATER CHICAGO**

NORTH SIDE SEWAGE TREATMENT WORKS

CONTRACT 78-020-CP
SECONDARY TREATMENT FACILITIES

BORING LOCATION PLAN

Designed D.W. | Drawn Z.B. | Checked R.W.B. | Reviewed | DATE: APR 10 2008 | SHEET NO 2C-39

Correct	Assistant Chief Engineer Chief Engineer
Approved	
Approved	
SCALES SHOWN ARE SCALES OF TRACINGS	

FEC - 1

FEC - 2

47

WESTENHOFF & NOVICK, INC		CONSULTING ENGINEERS			
FIELD BORING LOG					
SHEET 1 OF 2					
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.					
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. SSC-1					
BORING CONTRACTOR Raymond International TYPE RIG CNE LOCATION					
SOILS ENGR. C. Machnic INSPECTOR J. Tocco DRILLER D. FERRARI STRUCTURE					
GROUND WATER OBSERVATIONS					
AT 14.0 FT DURING DRILLING TYPE SS CASING SAMPLER CORE BARREL LINE & STA					
AT 15.0 FT AFTER 0 HRS SIZE ID 1-3/8" OFFSET SURFACE ELEV 22.87					
AT 16.0 FT AFTER 125 HRS HAMMER WT 140 LB. DATE START 5-26-77					
AT 17.0 FT AFTER 30" HRS HAMMER FALL 30" DATE FINISH 5-26-77					
DEPTH	CASING	SAMPLE	BLOWS PER		
BELOW	DEPTHS	ON SAMPLER	FOOT		
SURFACE PER FT FROM TO 0-616-02-8					
INDICATE ELEVATION OF STRATA CHANGE					
SOIL IDENTIFICATION & DRILLER'S NOTES					
NO. & TYPE PER REC.					
5	1-2.5	2 2 4	4	Fill: dk Gr & Yel-Bk Clayey SILT and Yel-Bk & Bk SAND, little f-c Gravel; blk cinder noted, Silt layers noted, Gravel (fill) layer noted.	1.5 SS-1
	3.5-5.0	3 3 5	5		1.5 SS-2
	6-8.5	6 7 10	10		1.5 SS-3
	9.5-10			Very Stiff Yel-Bk mottled Gr Silty CLAY, little f-c Sand, trace f-m Gravel; Silt layers noted.	NR
	11-13.5				4.0 ST-4 30" 20"
	13.5-15.5	5 7 9	9	Medium to Stiff Gr Clayey SILT, little f-c Sand, trace f. Gravel.	1.75 SS-5
	16-18.5			Soft Gr Silty CLAY, little f-c Sand, trace f. Gravel.	1.5 ST-6 30" 25"
	18.5-20	2 2 2	2		1.5 SS-7
REMARKS: NR - No Recovery				BORING NO. FEC-1	SHEET 1 OF 2

WESTENHOFF & NOVICK, INC		CONSULTING ENGINEERS			
FIELD BORING LOG					
SHEET 2 OF 2					
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.					
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. FEC-1					
BORING CONTRACTOR Raymond International TYPE RIG CNE LOCATION					
SOILS ENGR. C. Machnic INSPECTOR J. Tocco DRILLER D. FERRARI STRUCTURE					
GROUND WATER OBSERVATIONS					
AT 14.0 FT DURING DRILLING TYPE SS CASING SAMPLER CORE BARREL LINE & STA					
AT 15.0 FT AFTER 0 HRS SIZE ID 1-3/8" OFFSET SURFACE ELEV 22.87					
AT 16.0 FT AFTER 125 HRS HAMMER WT 140 LB. DATE START 5-26-77					
AT 17.0 FT AFTER 30" HRS HAMMER FALL 30" DATE FINISH 5-26-77					
DEPTH	CASING	SAMPLE	BLOWS PER		
BELOW	DEPTHS	ON SAMPLER	FOOT		
SURFACE PER FT FROM TO 0-616-02-8					
INDICATE ELEVATION OF STRATA CHANGE					
SOIL IDENTIFICATION & DRILLER'S NOTES					
NO. & TYPE PER REC.					
25	21-23.5			Medium Gr Silty CLAY, little f-c Sand, trace f. Gravel.	2.5 SS-9
	23.5-25	2 2 3	3		1.5 ST-10 30" 20"
	26-28.5			Gr f-c SAND, little f-m Gravel, little Silt, trace Clay.	1.5 ST-11 30" 20"
	28.5-30	4 4 5	5	Stiff Gr Silty CLAY, little f-c Sand, trace f. Gravel.	1.5 SS-11
REMARKS: End of Boring.				BORING NO. FEC-1	SHEET 2 OF 2

WESTENHOFF & NOVICK, INC		CONSULTING ENGINEERS			
FIELD BORING LOG					
SHEET 1 OF 2					
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.					
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. FEC-2					
BORING CONTRACTOR Raymond International TYPE RIG CNE LOCATION					
SOILS ENGR. C. Machnic INSPECTOR J. Tocco DRILLER D. FERRARI STRUCTURE					
GROUND WATER OBSERVATIONS					
AT 20.0 FT DURING DRILLING TYPE SS CASING SAMPLER CORE BARREL LINE & STA					
AT 21.0 FT AFTER 0 HRS SIZE ID 1-3/8" OFFSET SURFACE ELEV 22.75					
AT 22.0 FT AFTER 168 HRS HAMMER WT 140 LB. DATE START 6-8-77					
AT 23.0 FT AFTER 30" HRS HAMMER FALL 30" DATE FINISH 6-8-77					
DEPTH	CASING	SAMPLE	BLOWS PER		
BELOW	DEPTHS	ON SAMPLER	FOOT		
SURFACE PER FT FROM TO 0-616-02-8					
INDICATE ELEVATION OF STRATA CHANGE					
SOIL IDENTIFICATION & DRILLER'S NOTES					
NO. & TYPE PER REC.					
5	1-2.5	6 7 12	12	Fill: Bk, Yel-Bk & Gr Silty CLAY, little f-c Sand, trace f-c Gravel; cinders, roots, wood, and organic material noted; Silt seams and pockets noted, Sand layer at 18'.	1.5 SS-1
	3.5-5	5 6 8	8		4.5 SS-2
	6-8.5				2.0 ST-3 30" 12"
	9.5-10	3 4 5	5		1.1 SS-4
	11-13.5				3.0 ST-5 30" 20"
	13.5-15	2 3 4	4		1.1 SS-6
	16-18.5				1.5 ST-7 30" 11"
	18.5-20	7 15 24	24		1.5 SS-8
REMARKS:				BORING NO. FEC-2	SHEET 1 OF 2

WESTENHOFF & NOVICK, INC		CONSULTING ENGINEERS			
FIELD BORING LOG					
SHEET 2 OF 2					
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.					
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. SSC-3					
BORING CONTRACTOR Raymond International TYPE RIG CNE LOCATION					
SOILS ENGR. C. Machnic INSPECTOR J. Tocco DRILLER D. FERRARI STRUCTURE					
GROUND WATER OBSERVATIONS					
AT 20.0 FT DURING DRILLING TYPE SS CASING SAMPLER CORE BARREL LINE & STA					
AT 21.0 FT AFTER 0 HRS SIZE ID 1-3/8" OFFSET SURFACE ELEV 22.75					
AT 22.0 FT AFTER 168 HRS HAMMER WT 140 LB. DATE START 6-8-77					
AT 23.0 FT AFTER 30" HRS HAMMER FALL 30" DATE FINISH 6-8-77					
DEPTH	CASING	SAMPLE	BLOWS PER		
BELOW	DEPTHS	ON SAMPLER	FOOT		
SURFACE PER FT FROM TO 0-616-02-8					
INDICATE ELEVATION OF STRATA CHANGE					
SOIL IDENTIFICATION & DRILLER'S NOTES					
NO. & TYPE PER REC.					
25	21-23.5			Soft Gr Silty CLAY, little f-c Sand, trace f. Gravel; blk Silty Clay pockets noted, Silt layers noted.	2.5 ST-9 30" 30"
	23.5-25	2 2 2	2		3.5 SS-10
	26-28.5				1.5 ST-11 30" 30"
	28.5-30	2 3 4	4	Medium Gr Silty CLAY, little f-c Sand, trace f. Gravel.	1.75 SS-12
REMARKS: End of Boring.				BORING NO. FEC-2	SHEET 2 OF 2

WESTENHOFF & NOVICK, INC		CONSULTING ENGINEERS			
FIELD BORING LOG					
SHEET 1 OF 2					
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.					
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. FEC-3					
BORING CONTRACTOR Raymond International TYPE RIG CNE LOCATION					
SOILS ENGR. C. Machnic INSPECTOR J. Tocco DRILLER D. FERRARI STRUCTURE					
GROUND WATER OBSERVATIONS					
AT 25.0 FT DURING DRILLING TYPE SS CASING SAMPLER CORE BARREL LINE & STA					
AT 26.0 FT AFTER 0 HRS SIZE ID 1-3/8" OFFSET SURFACE ELEV 20.54					
AT 27.0 FT AFTER 168 HRS HAMMER WT 140 LB. DATE START 6-8-77					
AT 28.0 FT AFTER 30" HRS HAMMER FALL 30" DATE FINISH 6-8-77					
DEPTH	CASING	SAMPLE	BLOWS PER		
BELOW	DEPTHS	ON SAMPLER	FOOT		
SURFACE PER FT FROM TO 0-616-02-8					
INDICATE ELEVATION OF STRATA CHANGE					
SOIL IDENTIFICATION & DRILLER'S NOTES					
NO. & TYPE PER REC.					
5	1-2.5	4 4 5	5	Fill: Bk, Yel-Bk & Gr Silty CLAY, little f-c Sand, trace f-m Gravel; Silt seams and pockets noted, thin blk Silty Clay noted.	1.5 SS-1
	3.5-5.5	3 3 4	4		NR
	6-8.5				1.7 ST-2 36" 12"
	8.5-10	2 3 4	4	Medium Gr mottled Yel-Bk Silty CLAY, trace f-c Sand, trace f. Gravel.	2.1 ST-3
	11-13.5				1.0 ST-4 36" 20"
	13.5-15	3 1 5	5	Medium Gr Clayey Silt, little f-c Sand, trace f. Gravel; pink Silty-Clay pockets noted, Silty Clay and Sand layers noted.	1.6 SS-5
	16-18.5				1.5 ST-6 36" 30"
	18.5-20	2 2 2	2	Soft Gr Silty CLAY, little f-c Sand, trace f. Gravel; pink Silty Clay pockets noted.	1.5 ST-7
REMARKS: NR - No Recovery				BORING NO. FEC-3	SHEET 1 OF 2

WESTENHOFF & NOVICK, INC		CONSULTING ENGINEERS			
FIELD BORING LOG					
SHEET 2 OF 2					
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.					
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. FEC-3					
BORING CONTRACTOR Raymond International TYPE RIG CNE LOCATION					
SOILS ENGR. C. Machnic INSPECTOR J. Tocco DRILLER D. FERRARI STRUCTURE					
GROUND WATER OBSERVATIONS					
AT 25.0 FT DURING DRILLING TYPE SS CASING SAMPLER CORE BARREL LINE & STA					
AT 26.0 FT AFTER 0 HRS SIZE ID 1-3/8" OFFSET SURFACE ELEV 20.54					
AT 27.0 FT AFTER 168 HRS HAMMER WT 140 LB. DATE START 6-8-77					
AT 28.0 FT AFTER 30" HRS HAMMER FALL 30" DATE FINISH 6-8-77					
DEPTH	CASING	SAMPLE	BLOWS PER		
BELOW	DEPTHS	ON SAMPLER	FOOT		
SURFACE PER FT FROM TO 0-616-02-8					
INDICATE ELEVATION OF STRATA CHANGE					
SOIL IDENTIFICATION & DRILLER'S NOTES					
NO. & TYPE PER REC.					
25	21-23.5				2.5 ST-8 36" 30"
	23.5-25	2 2 2	2	Medium Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	2.5 SS-9
	26-28.5				1.4 ST-10 36" 30"
	28.5-30	2 2 3	3	End of Boring.	1.4 SS-11
REMARKS:				BORING NO. FEC-3	SHEET 2 OF 2

REVISIONS			THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 78-020-CP SECONDARY TREATMENT FACILITIES BORING LOGS		Correct Approved Assistant Chief Engineer Analyzed Chief Engineer
NO.	DATE	BY			
Designed D.W. Drawn Checked R.W.S. Reviewed			DATE: APR., 1986		SHEET NO. 2C-43

TFB-1a

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WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 1 OF 1
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. ST-1
BORING CONTRACTOR Raymond International TYPE RIG CHE LOCATION
SOILS ENGR. C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 2.0 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 23.24
AT 2.0 FT AFTER 0 MRS SIZE ID 1-3/8" SURFACE ELEV 22.05
AT 7.0 FT AFTER 31 MRS HAMMER WT 140 LB DATE START 5/26/77
AT 7.0 FT AFTER 31 MRS HAMMER FALL 30" DATE FINISH 5/26/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS	BLOWS PER 6" ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE	PEN REC
1-2.5	6	9	11	Fine Blk, Yel-Bk & Gr Silty CLAY, little f-c Sand, trace f-m Gravel; cinders and Silt layers noted.	4.54 SS-1	
3.5-5.4	2	3	4		2.55 SS-2	
6-8.5					1.55 ST-3 30" 16"	
9.5-10	2	2	2		2.55 SS-4	
11-13.5				Very Stiff Gr mottled Reddish Yel-Bk Silty CLAY, little f-c Sand, trace f-m Gravel.	2.25 ST-5 30" 24"	
13.5-15	5	7	8	Stiff Gr Clayey SILT, little f-c Sand, trace f-m Gravel.	2.25 SS-6	
16-18.5					.5 ST-7 30" 30"	
18.5-20	2	2	3	Medium Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	.6 SS-8	

REMARKS: BORING NO. ST-1
SHEET 1 OF 1

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 2 OF 2
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. ST-1
BORING CONTRACTOR Raymond International TYPE RIG CHE LOCATION
SOILS ENGR. C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 23.0 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 23.24
AT 23.0 FT AFTER 0 MRS SIZE ID 1-3/8" SURFACE ELEV 22.05
AT 27.0 FT AFTER 31 MRS HAMMER WT 140 LB DATE START 5/26/77
AT 27.0 FT AFTER 31 MRS HAMMER FALL 30" DATE FINISH 5/26/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS	BLOWS PER 6" ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE	PEN REC
21-23.5				Soft Gr. Silty CLAY, little f-c Sand, trace f-m Gravel.	2.55 ST-9 30" 30"	
23.5-25	1	1	2		2.55 SS-10	
26-28.5				Medium Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	4.55 ST-11 30" 30"	
28.5-30	2	2	3	End of Boring.	4.55 SS-12	

REMARKS: BORING NO. ST-1
SHEET 2 OF 2

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 1 OF 1
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-1
BORING CONTRACTOR Raymond International TYPE RIG CHE LOCATION
SOILS ENGR. C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 22.0 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 22.05
AT 4.5 FT AFTER 1 MRS SIZE ID 1-3/8" SURFACE ELEV 22.05
AT 4.5 FT AFTER 1 MRS HAMMER WT 140 LB DATE START 5/26/77
AT 6.66 FT AFTER 336 MRS HAMMER FALL 30" DATE FINISH 5/26/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS	BLOWS PER 6" ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE	PEN REC
1.0-2.5	3	4	6	Blk, Gr & Yel-Bk Silty CLAY, little f-c Sand, trace f-m Gravel; blk Silty Clay seams noted, Silt seams noted and roots noted.	4.54 SS-1	
3.5-5.0	3	4	6		2.0 SS-2	
6.0-8.5				Stiff Blk Organic Silty CLAY, trace f-m Sand; roots and Sand seams noted.	1.25 ST-3 30" 19"	
8.5-10.0	2	4	4		.55 SS-4	
11.0-13.5				Gr mottled Yel-Bk Silty CLAY, little f-c Sand, trace f-m Gravel; pink Silty Clay pockets noted, Sand seams noted.	2.0 ST-5 30" 25"	
13.5-15.0	2	1	4	Soft Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	NR	
16.0-18.5					2.5 ST-6 30" 30"	
18.5-20.0	1	1	2		.2 SS-7	

REMARKS: NR - No recovery BORING NO. TFB-1
SHEET 1 OF 1

TFB-1b

TFB-1c

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 2 OF 3
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-1
BORING CONTRACTOR Raymond International TYPE RIG CHE LOCATION
SOILS ENGR. C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 22.0 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 22.05
AT 4.5 FT AFTER 1 MRS SIZE ID 1-3/8" SURFACE ELEV 22.05
AT 4.5 FT AFTER 1 MRS HAMMER WT 140 LB DATE START 5/26/77
AT 6.66 FT AFTER 336 MRS HAMMER FALL 30" DATE FINISH 5/26/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS	BLOWS PER 6" ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE	PEN REC
21.0-23.5					2.2 ST-8 30" 28"	
23.5-25.0	1	2	2		2.2 SS-9	
26.0-28.5				Medium Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	2.5 ST-10 30" 28"	
28.5-30.0	2	2	2		4.11 SS-11	
31.0-33.5				Medium to Stiff Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	1.612 SS-12 30" 28"	
33.5-35.0	5	7	8	Medium to Stiff Gr Clayey SILT, little to some f-c Sand, trace f-m Gravel.	2.25 SS-13	
36.0-38.5					.75 ST-14 30" 30"	
38.5-40.0	5	7	8		.75 SS-15	

REMARKS: BORING NO. TFB-1
SHEET 2 OF 3

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 3 OF 3
PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, Ill.
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-1
BORING CONTRACTOR Raymond International TYPE RIG CHE LOCATION
SOILS ENGR. C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 22.0 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 22.05
AT 4.5 FT AFTER 1 MRS SIZE ID 1-3/8" SURFACE ELEV 22.05
AT 4.5 FT AFTER 1 MRS HAMMER WT 140 LB DATE START 5/26/77
AT 6.66 FT AFTER 336 MRS HAMMER FALL 30" DATE FINISH 5/26/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS	BLOWS PER 6" ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE	PEN REC
41.0-43.5				Medium to Stiff Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	1.0 ST-16 30" 26"	
43.5-45.0	3	4	5		.9 SS-17	
46.0-48.5				Dense to Very Dense Gr SILTY, some f-c Sand, little f-m Gravel.	4.54 ST-18 30" 18"	
48.5-50.0	15	15	22		SS-19	
51.0-52.5	20	29	37	Very Dense Gr Clayey SILT, little f-c Sand, trace f-m Gravel; 9f silt seams and pockets noted.	2.0 SS-20	
53.5-55.0	18	24	31		2.0 SS-21	
56.0-57.5	27	32	44	Very Dense Gr SILTY, some f-c Sand, little f-m Gravel, trace Clay; seams of gr. Clayey SILT noted.	4.54 SS-22	
58.5-60.0	29	39	27	End of Boring	4.54 SS-23	

REMARKS: BORING NO. TFB-1
SHEET 3 OF 3

RETA ENGINEERS / A JOINT VENTURE CHICAGO

REVISIONS			THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO		Correct
NO.	DATE	BY			
			NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 78-020-CP SECONDARY TREATMENT FACILITIES BORING LOGS		Approved: Approved: Assistant Chief Engineer Chief Engineer
			BORING LOGS		
			Designed D.W.	Drawn	Checked R.W.B.
			Reviewed	DATE APR., 1986	SHEET NO 2C-65

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 1 OF 2

PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-2

BORING CONTRACTOR Raymond International TYPE RIS CHE LOCATION
SOILS ENGR C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 9' FT DURING DRILLING TYPE SS OFFSET
AT 24.00 FT AFTER 3 HRS SIZE ID 1-3/8" SURFACE ELEV 22.16
AT 5.50 FT AFTER 96 HRS HAMMER WT 140 lbs DATE START 5/19/77
AT 1' FT AFTER HRS HAMMER FALL 30" DATE FINISH 5/19/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	INDICATE ELEVATION OF STRATA CHANGE	SAMPLE NO & TYPE	PER	REC
1.0-2.5	6	8	10	FINE: Blk, Yel-Br & Gr Silty CLAY, little f-c Sand, trace f Gravel; hair roots and decayed wood noted; thin Sand seams and Silt pockets noted.		4.5	SS-1	
3.5-5.0	5	6	8			2.25	SS-2	
6.0-8.5				Stiff Blk organic CLAY, little f-c Sand, trace f Gravel; pest and roots noted.		2.75	ST-3	30" 15"
9.5-10.0	4	5	6	Stiff Gr mottled Yel-Br Silty CLAY, trace f Gravel; pink Silty Clay pockets noted; Silt seams noted.		1.0	SS-4	
11.0-13.5				Very Stiff Gr Clayey SILT, little f-c Sand, trace f Gravel.		1.75	ST-5	30" 26"
13.5-18.5	3	5	6			1.75	SS-6	
16.0-18.5				Soft Gr Silty CLAY, little f-c Sand, trace f Gravel; pink Silty Clay pockets noted.		1.2	ST-7	30" 10"
18.5-20.0	1	1	2			1.2	SS-8	

REMARKS: BORING NO. TFB-2
SHEET 1 OF 2

TFB-3a

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 2 OF 2

PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-2

BORING CONTRACTOR Raymond International TYPE RIS CHE LOCATION
SOILS ENGR C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 24.00 FT AFTER 3 HRS SIZE ID 1-3/8" SURFACE ELEV 22.16
AT 5.50 FT AFTER 96 HRS HAMMER WT 140 lbs DATE START 5/19/77
AT 1' FT AFTER HRS HAMMER FALL 30" DATE FINISH 5/19/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	INDICATE ELEVATION OF STRATA CHANGE	SAMPLE NO & TYPE	PER	REC
21.0-23.5						2	ST-9	30" 29"
23.5-25.0	1	1	2	Soft Gr Silty CLAY, little f-c Sand, trace f Gravel; pink Silty Clay pockets noted.		2.5	SS-10	
26.0-28.5						2.5	ST-11	30" 22"
30.5-30.0	1	2	2			2	SS-12	
31.0-33.5				Medium Gr Silty CLAY, little f-c Sand, trace f Gravel.		2.5	ST-13	30" 21"
33.5-35.0	2	3	4			1.6	SS-14	
36.0-38.5				Stiff Gr Silty CLAY, little f-c Sand, trace f Gravel.		1.7	ST-15	30" 30"
38.5-40.0	3	4	5	End of Boring		1.0	SS-16	

REMARKS: BORING NO. TFB-2
SHEET 2 OF 2

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 1 OF 2

PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-1

BORING CONTRACTOR Raymond International TYPE RIS CHE LOCATION
SOILS ENGR C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 24.00 FT AFTER 3 HRS SIZE ID 1-3/8" SURFACE ELEV 21.52
AT 4.50 FT AFTER 360 HRS HAMMER WT 140 lbs DATE START 5/25/77
AT 1' FT AFTER HRS HAMMER FALL 30" DATE FINISH 5/25/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	INDICATE ELEVATION OF STRATA CHANGE	SAMPLE NO & TYPE	PER	REC
1.0-2.5	7	9	5	FINE: Ye'-Br, Gr & Blk Silty CLAY, little f-c Sand, trace f Gravel; blk Silty Clay seams and roots noted; Silt pockets noted.		4.5	SS-1	
3.5-5.0	2	3	4			1.8	SS-2	
6.0-8.5				Stiff Blk Organic CLAY, trace f-c Sand, trace f Gravel; Sand pockets and roots noted.		7.5	ST-3	30" 12"
8.5-10.0	4	5	6	Stiff Yel-Br mottled Gr Silty CLAY, trace f-c Sand, trace f Gravel; pink Silty Clay pockets noted.		1.25	SS-4	
11.0-13.5				Stiff Gr Clayey SILT, little f-c Sand, trace f Gravel.		1.5	ST-5	30" 18"
13.5-15.0	1	2	2			7.5	SS-6	
16.0-18.5				Soft Gr Silty CLAY, little f-c Sand, trace f Gravel; pink Silty Clay pockets noted.		2.5	ST-7	30" 30"
18.5-20.0	1	1	1			2.5	SS-8	

REMARKS: BORING NO. TFB-1
SHEET 1 OF 2

TFB-3b

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 2 OF 2

PROJECT NO. 2003 PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-1

BORING CONTRACTOR Raymond International TYPE RIS CHE LOCATION
SOILS ENGR C. Machnich INSPECTOR J. Trezzo DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 24.00 FT AFTER 3 HRS SIZE ID 1-3/8" SURFACE ELEV 21.52
AT 4.50 FT AFTER 360 HRS HAMMER WT 140 lbs DATE START 5/25/77
AT 1' FT AFTER HRS HAMMER FALL 30" DATE FINISH 5/25/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	INDICATE ELEVATION OF STRATA CHANGE	SAMPLE NO & TYPE	PER	REC
21.0-23.5						2.5	ST-9	30" 29"
23.5-25.0	1	1	2			2.5	SS-10	
26.0-28.5						2.5	ST-11	30" 30"
28.5-30.0	3	3	4	Medium Gr Clayey SILT, little f-c Sand, trace f Gravel.		2.5	SS-12	
31.0-33.5				Medium Gr Silty CLAY, little f-c Sand, trace f Gravel.		5	ST-13	30" 30"
33.5-35.0	2	3	4			5	SS-14	
36.0-38.5				Stiff Gr Silty CLAY, little f-c Sand, trace f Gravel.		1.9	ST-15	30" 20"
38.5-40.0	4	5	5	End of Boring		1.0	SS-16	

REMARKS: BORING NO. TFB-1
SHEET 2 OF 2

REVISIONS			THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO		Correct
NO.	DATE	BY			
			NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 78-020-CP SECONDARY TREATMENT FACILITIES		Approved _____ Assistant Chief Engineer
			BORING LOGS		
			DESIGNED D.W. DRAWN _____ CHECKED R.W.B. REVIEWED _____		SCALES SHOWN ARE SCALES OF TRACINGS
			DATE APR., 1986		SHEET NO. 2C-66

TFB-4

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 1 OF 3

PROJECT NO. 2003 PROJECT NAME A LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-4

BORING CONTRACTOR Raymond International, Inc. TYPE MS CHE LOCATION
SOLS ENGR C. Machnich INSPECTOR J. Tesoro DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 12 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 22.02
AT 10 FT AFTER 0 HRS SIZE ID 1-3/8" DATE START 5/23/77
AT 4.60 FT AFTER 48 HRS HAMMER WT 140 lbs DATE FINISH 5/23/77
AT 1 FT AFTER HRS HAMMER FALL 30"

DEPTH BELOW SURFACE PER FT	CASING BLOWS	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE PER REC.
1.0-2.5	3	4	4	FILL: Blk, Yel-br & Gr Silty CLAY, little f-c Sand, trace f Gravel; Silt seams noted.	1.1 SS-1
3.5-5.0	2	3	4		7.5 SS-2
6.0-8.5				Stiff Blk Organic CLAY, trace f-m Sand; Silt pockets noted.	1.1 ST-3 30" 16"
8.5-10.0	3	3	2	Stiff to Very Stiff Gr mottled Yel-br Silty CLAY, little f-c Sand, trace f Gravel; Clayey Silt layer noted, roots noted and pink Silty Clay pockets noted.	7.5 SS-4
11.0-13.5					SS-5 10" 21"
13.5-15.0	2	3	3		7.5 SS-6
16.0-18.5				Soft Gr Silty CLAY, little f-c Sand, trace f-m Gravel; pink Silty Clay pockets noted, Gr Clayey Silt layer noted at 19".	2.5 ST-7 30" 30"
18.5-20.0	1	2	2		2.5 SS-8

REMARKS: BORING NO. TFB-4 SHEET 1 OF 3

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 2 OF 3

PROJECT NO. 2003 PROJECT NAME A LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-4

BORING CONTRACTOR Raymond International, Inc. TYPE MS CHE LOCATION
SOLS ENGR C. Machnich INSPECTOR J. Tesoro DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 12 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 22.02
AT 10 FT AFTER 0 HRS SIZE ID 1-3/8" DATE START 5/23/77
AT 4.60 FT AFTER 48 HRS HAMMER WT 140 lbs DATE FINISH 5/23/77
AT 1 FT AFTER HRS HAMMER FALL 30"

DEPTH BELOW SURFACE PER FT	CASING BLOWS	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE PER REC.
21.0-23.5					2.5 SS-9 30" 30"
23.5-25.0	1	1	2		2.5 SS-10
26.0-28.5				Medium Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	4 ST-11 30" 30"
28.5-30.0	1	2	3	Stiff Gr Clayey SILT, little to some f-c Sand, trace f Gravel.	7.5 SS-12
31.0-33.5					SS-13 30" 28"
33.5-40.0	3	4	6		1.0 SS-14
36.0-38.5				Stiff Gr Silty CLAY, little f-c Sand, trace f Gravel; pink Silty Clay pockets noted at 43".	1.25 ST-15 30" 26"
38.5-40.0	4	5	6		1.2 SS-16

REMARKS: BORING NO. TFB-4 SHEET 2 OF 3

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 3 OF 3

PROJECT NO. 2003 PROJECT NAME A LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-4

BORING CONTRACTOR Raymond International, Inc. TYPE MS CHE LOCATION
SOLS ENGR C. Machnich INSPECTOR J. Tesoro DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 19 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 22.02
AT 10 FT AFTER 0 HRS SIZE ID 1-3/8" DATE START 5/23/77
AT 4.60 FT AFTER 48 HRS HAMMER WT 140 lbs DATE FINISH 5/23/77
AT 1 FT AFTER HRS HAMMER FALL 30"

DEPTH BELOW SURFACE PER FT	CASING BLOWS	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE PER REC.
41.0-43.5					1.2 ST-17 30" 27"
43.5-45.0	1	4	5	Hard Gr Clayey SILT, some f-c Sand, trace f-m Gravel; Sand layer noted.	2.5 SS-18
46.0-48.5					4.54 ST-19 30" 20"
48.5-50.0	15	19	23	Hard Gr Silty CLAY, little f-c Sand, trace f Gravel.	4.54 SS-20
51.0-53.5	9	17	28		1.0 SS-21
53.5-55.0	21	25	33		2.5 SS-22
56.0-58.5	17	25	4	Very Dense Gr SILT; little f-c Sand, trace Clay trace f-m Gravel.	4.5 SS-23
58.5-60.0	110			End of Boring	NR

REMARKS: NR - No Recovery BORING NO. TFB-4 SHEET 3 OF 3

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 1 OF 3

PROJECT NO. 2003 PROJECT NAME A LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-5

BORING CONTRACTOR Raymond International, Inc. TYPE MS CHE LOCATION
SOLS ENGR C. Machnich INSPECTOR J. Tesoro DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 9 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 21.99
AT 5.17 FT AFTER 28 HRS HAMMER WT 140 lbs DATE START 5/24/77
AT 1 FT AFTER HRS HAMMER FALL 30"

DEPTH BELOW SURFACE PER FT	CASING BLOWS	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE PER REC.
1.0-2.5	3	4	4	FILL: Yel-br, Blk & Gr Silty CLAY, trace to little f-c Sand, trace f Gravel; roots and blk Silty Clay layers noted, Sand pockets noted.	2.25 SS-1
3.5-5.2	2	3	4		NR
6.0-8.5				Stiff Blk Organic CLAY, trace f-c Sand, trace f Gravel; br Silt seams noted.	7 ST-2 30" 13"
8.5-10.0	3	4	4	Stiff to Very Stiff Gr mottled Yel-br Silty CLAY, little f-c Sand, trace f Gravel.	NR
11.0-13.5					3.2 ST-3 30" 18"
13.5-15.0	4	4	5	Medium Gr Silty CLAY, little f-c Sand, trace f Gravel; gr Clayey Silt layer at 14"; pink Silty Clay pockets noted.	8 SS-4
16.0-18.5					4 ST-5 30" 30"
18.5-20.0	1	1	2		2.5 SS-6

REMARKS: NR - No recovery BORING NO. TFB-5 SHEET 1 OF 3

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 3 OF 3

PROJECT NO. 2003 PROJECT NAME A LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-5

BORING CONTRACTOR Raymond International, Inc. TYPE MS CHE LOCATION
SOLS ENGR C. Machnich INSPECTOR J. Tesoro DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 9 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 21.99
AT 5.17 FT AFTER 28 HRS HAMMER WT 140 lbs DATE START 5/24/77
AT 1 FT AFTER HRS HAMMER FALL 30"

DEPTH BELOW SURFACE PER FT	CASING BLOWS	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE PER REC.
21.0-23.5				Soft Gr Silty CLAY, little f-c Sand, trace f-m Gravel; pink Silty Clay pockets noted.	1.5 ST-7 30" 30"
23.5-25.0	2	2	3		4 SS-8
26.0-28.5				Medium Gr Silty CLAY, little f-c Sand, trace f-m Gravel; pink Silty Clay pockets noted.	4 ST-9 30" 29"
28.5-30.0	2	2	2		7.5 SS-10
31.0-33.5				Stiff Gr. Clayey SILT, little f-c Sand, trace f Gravel.	8 ST-11 30" 25"
33.5-35.0	2	4	5		8 SS-12
36.0-38.5					NR
38.5-40.0	7	10	12	Stiff Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	1.0 SS-13

REMARKS: BORING NO. TFB-5 SHEET 3 OF 3

WESTENHOFF & NOVICK, INC. CONSULTING ENGINEERS
FIELD BORING LOG SHEET 1 OF 3

PROJECT NO. 2003 PROJECT NAME A LOCATION North Side Sewage Treatment Works, Skokie, IL
CLIENT Metropolitan Sanitary District of Greater Chicago BORING NO. TFB-5

BORING CONTRACTOR Raymond International, Inc. TYPE MS CHE LOCATION
SOLS ENGR C. Machnich INSPECTOR J. Tesoro DRILLER D. Ferrara STRUCTURE

GROUND WATER OBSERVATIONS CASING SAMPLER CORE BARREL LINE & STA
AT 9 FT DURING DRILLING TYPE SS OFFSET SURFACE ELEV 21.99
AT 5.17 FT AFTER 28 HRS HAMMER WT 140 lbs DATE START 5/24/77
AT 1 FT AFTER HRS HAMMER FALL 30"

DEPTH BELOW SURFACE PER FT	CASING BLOWS	SAMPLE DEPTHS FROM-TO	BLOWS PER FT ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO & TYPE PER REC.
41.0-43.5					1.0 ST-14 30" 29"
43.5-45.0	7	8	10	Very Stiff Gr Clayey SILT, some f-c Sand, trace f-m Gravel.	3.0 SS-15
46.0-48.5					5.54 ST-16 30" 11"
48.5-50.0	12	16	22	Hard Gr Silty CLAY, little f-c Sand, trace f Gravel.	4.54 SS-17
51.0-52.5	19	27	32		4.54 SS-18
53.5-55.0	25	33	41	Very Dense Gr SILT, trace to little f-c Sand, trace Clay, trace f Gravel.	4.54 SS-19
56.0-57.5	12	18	31		4.54 SS-20
58.5-60.0	20	32	39	End of Boring	4.54 SS-21

REMARKS: BORING NO. TFB-5 SHEET 1 OF 3

RETA ENGINEERS / A JOINT VENTURE CHICAGO

REVISIONS			THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 78-020-CP SECONDARY TREATMENT FACILITIES BORING LOGS		Correct Approved Approved Chief Engineer
NO.	DATE	BY			
				Designed D.W. Drawn Checked R.W.B. Reviewed	SCALES SHOWN ARE SCALES OF TRACINGS

TFB-6

WESTENHOFF & NOVICK, INC.		FIELD BORING LOG		CONSULTING ENGINEERS	
PROJECT NO. 2003		PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, IL		SHEET 2 OF 2	
CLIENT Metropolitan Sanitary District of Greater Chicago		BORING NO. TFB-6			
BORING CONTRACTOR Raymond International Type INC		LOCATION			
SOILS ENGR. C. Machnich		INSPECTOR J. Trezzo		DRILLER D. Ferrara	
GROUND WATER OBSERVATIONS		CASING SAMPLER CORE BARREL		LINE & STA	
AT SURF. FT.	DURING DRILLING	TYPE	SS	OFFSET	21.30
AT 3.5 FT. AFTER 0 WPS	SIZE ID	1-3/8"		SURFACE ELEV	21.30
AT 4.17 FT. AFTER 360 WPS	HAMMER WT	140 lbs		DATE START	5/25/77
AT 30 FT. AFTER WPS	HAMMER FALL	30"		DATE FINISH	5/25/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS FROM-TO	BLOWS PER 4' ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO. & TYPE	PEN REC.
1.0-2.5	4	5	8	FILLS: blk. Gr & Yel-Bk Silty CLAY, little f-c Sand, trace f Gravel; blk Silty Clay seams noted, blk cinders noted.	1.0 SS-1	
3.5-5.0	3	3	4		2.5 SS-2	
6.0-8.5				Stiff blk Organic Silty CLAY, trace f-c Sand, trace f Gravel; Silt lenses noted.	1.0 ST-3 30" 13"	
9.5-10.0	2	3	4	Very Stiff Gr mottled Yel-Bk Silty CLAY, little f-c Sand, trace f-m Gravel; Sand lenses noted, clayey Silt layer noted at 12'.	20 SS-4	
11.0-13.5					28 ST-5 30" 20"	
13.5-14.0	2	3	4	SOFT Gr Silty CLAY, little f-c Sand, trace f Gravel; pink Silty Clay pockets noted.	25 SS-6	
16.0-18.5					1.25 ST-7 30" 29"	
18.5-20.0	2	2	1		25 SS-8	

REMARKS: _____ BORING NO. TFB-6
SHEET ____ OF ____

WESTENHOFF & NOVICK, INC.		FIELD BORING LOG		CONSULTING ENGINEERS	
PROJECT NO. 2003		PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, IL		SHEET 2 OF 2	
CLIENT Metropolitan Sanitary District of Greater Chicago		BORING NO. TFB-6			
BORING CONTRACTOR Raymond International Type INC		LOCATION			
SOILS ENGR. C. Machnich		INSPECTOR J. Trezzo		DRILLER D. Ferrara	
GROUND WATER OBSERVATIONS		CASING SAMPLER CORE BARREL		LINE & STA	
AT SURF. FT.	DURING DRILLING	TYPE	SS	OFFSET	21.30
AT 3.5 FT. AFTER 0 WPS	SIZE ID	1-3/8"		SURFACE ELEV	21.30
AT 4.17 FT. AFTER 360 WPS	HAMMER WT	140 lbs		DATE START	5/25/77
AT 30 FT. AFTER WPS	HAMMER FALL	30"		DATE FINISH	5/25/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS FROM-TO	BLOWS PER 4' ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO. & TYPE	PEN REC.
21.0-23.5					25 ST-9 30" 30"	
23.5-25.0	1	1	2	Medium Gr Silty CLAY, little f-c Sand, trace f-m Gravel.	25 10	
26.0-28.5					75 ST-11 30" 30"	
28.5-30.0	3	4	6	Stiff Gr Clayey SILT, little f-c Sand, trace f Gravel.	1.0 12	
31.0-33.5					1.25 ST-11 30" 28"	
33.5-35.0	5	7	9	Stiff to Very Stiff Gr Silty CLAY, little f-c Sand, trace f-m Gravel; Silt seams noted.	HR	
36.0-38.5					1.25 ST-14 30" 22"	
38.5-40.0	7	9	11	End of Boring	1.6 15	

REMARKS: _____ BORING NO. TFB-6
SHEET ____ OF ____

WESTENHOFF & NOVICK, INC.		FIELD BORING LOG		CONSULTING ENGINEERS	
PROJECT NO. 2003		PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, IL		SHEET 1 OF 2	
CLIENT Metropolitan Sanitary District of Greater Chicago		BORING NO. TFB-7			
BORING CONTRACTOR Raymond International Type INC		LOCATION			
SOILS ENGR. C. Machnich		INSPECTOR J. Trezzo		DRILLER D. Ferrara	
GROUND WATER OBSERVATIONS		CASING SAMPLER CORE BARREL		LINE & STA	
AT SURF. FT.	DURING DRILLING	TYPE	SS	OFFSET	21.70
AT 3.5 FT. AFTER 0 WPS	SIZE ID	1-3/8"		SURFACE ELEV	21.70
AT 4.60 FT. AFTER 360 WPS	HAMMER WT	140 lbs		DATE START	5/25/77
AT 30 FT. AFTER WPS	HAMMER FALL	30"		DATE FINISH	5/25/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS FROM-TO	BLOWS PER 4' ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO. & TYPE	PEN REC.
1.0-2.5	3	3	3	FILLS: blk. Yel-Bk & Gr Silty CLAY, little f-c Sand, trace f Gravel; blk Silty Clay seams noted, blk cinders noted, Silt pockets noted.	2 25 SS-1	
3.5-5.0	1	2	1		1 25 SS-2	
5.0-8.5				Medium blk Organic Silty CLAY, trace f Gravel; Yel-Bk Silty Clay seams noted, Sand layer noted.	75 ST-3 30" 20"	
8.5-10.0	2	2	3	Very Stiff Yel-Bk mottled Gr Silty CLAY, little f-c Sand, trace f Gravel.	1.0 SS-4	
11.0-13.5					1.0 ST-5 30" 23"	
13.5-15.0	4	5	7	Stiff to Very Stiff Gr Clayey SILT, little f-c Sand, trace f Gravel.	1.5 SS-6	
16.0-18.5					1.5 ST-7 30" 30"	
18.5-20.0	3	4	5	Medium Gr Silty CLAY, little f-c Sand, trace f Gravel.	1.6 SS-8	

REMARKS: _____ BORING NO. TFB-7
SHEET ____ OF ____

WESTENHOFF & NOVICK, INC.		FIELD BORING LOG		CONSULTING ENGINEERS	
PROJECT NO. 2003		PROJECT NAME & LOCATION North Side Sewage Treatment Works, Skokie, IL		SHEET 2 OF 2	
CLIENT Metropolitan Sanitary District of Greater Chicago		BORING NO. TFB-7			
BORING CONTRACTOR Raymond International Type INC		LOCATION			
SOILS ENGR. C. Machnich		INSPECTOR J. Trezzo		DRILLER D. Ferrara	
GROUND WATER OBSERVATIONS		CASING SAMPLER CORE BARREL		LINE & STA	
AT SURF. FT.	DURING DRILLING	TYPE	SS	OFFSET	21.74
AT 3.5 FT. AFTER 0 WPS	SIZE ID	1-3/8"		SURFACE ELEV	21.74
AT 4.17 FT. AFTER 360 WPS	HAMMER WT	140 lbs		DATE START	5/25/77
AT 30 FT. AFTER WPS	HAMMER FALL	30"		DATE FINISH	5/25/77

DEPTH BELOW SURFACE	CASING BLOWS PER FT	SAMPLE DEPTHS FROM-TO	BLOWS PER 4' ON SAMPLER	SOIL IDENTIFICATION & DRILLERS NOTES	SAMPLE NO. & TYPE	PEN REC.
21.0-23.5					75 ST-8 30" 29"	
23.5-25.0	1	1	1		25 10	
26.0-28.5				Medium to Stiff Gr Clayey SILT, little f-c Sand, trace f-m Gravel; 1 coarse gravel noted.	75 ST-11 30" 30"	
28.5-30.0	2	2	3		75 ST-12	
31.0-33.5				Stiff Gr Silty CLAY, trace f-c Sand, trace f-m Gravel.	1.5 ST-13 30" 30"	
33.5-35.0	7	9	10		1.4 14	
36.0-38.5					9 15 30" 29"	
38.5-40.0	5	6	8	End of Boring	1.25 16	

REMARKS: _____ BORING NO. TFB-7
SHEET ____ OF ____

REVISIONS			THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO		Correct
NO.	DATE	BY			
			NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 78-020-CP SECONDARY TREATMENT FACILITIES BORING LOGS		Approved _____ Assistant Chief Engineer Approved _____ Chief Engineer
Designed B.W. Drawn _____ Checked K.W.B. Reviewed _____			DATE APR., 1986		SHEET NO. 2C-68

FEC-1

FEC-2a

WESTENHOFF & NOVICK INC.		SUMMARY OF SOIL TEST RESULTS												Project North Side Sewage Treatment Job No. 2003 Boring No. FEC-1 Page No. 1 of 2		
Sample Type No.	Depth ft.	N or S.P.T.	Unconf.-Comp.-t.s.f.		Wc %	γ _{dry} p.c.t.	L.L. %	P.L. %	Grain Size Analysis				Sp. Gravity	Soil Type Unified	Description	
			Test	Estimated					Gravel %	Sand %	Silt %	Clay %				
SS-1	1.0-2.5	6			13.5										Dk Gr & Yel-Br Clayey SILT and Gr SILT in layers and lenses, trace f-c Sand, trace f Gravel, cinders noted.	
SS-2	3.5-5.0	8													blk f-c SAND, little f-c Gravel, little silt; cinders noted.	
SS-3	6.0-7.5	17													Yel-Br & blk f-c SAND and f-m Gravel; little silt; cinders noted.	
ST-4	12.0-12.7	2.37	2.8	21.1	108.4	35.0	15.7								Yel-br mottled Gr Silty CLAY, little f-c Sand, trace f Gravel; silt layer and 1 medium Gravel.	
SS-5	13.5-15.0	*	4.5	13.8	123.5										Gr Clayey SILT, little f-c Sand, trace f Gravel.	
ST-6	17.3-16.1	0.75	0.7	19.9	112.5	26.8	14.1								Same as SS-5.	
SS-7	18.5-20.0	4	0.93	0.8	23.3	106.8									Gr Silty CLAY, little f-c Sand, trace f Gravel.	
ST-8	21.9-22.6	0.38	0.5	27.5	98.0	34.5	15.8								Gr Silty CLAY, little f-c Sand, trace f Gravel.	
SS-9	23.5-25.0	5			24.3										Same as SS-7.	
Remarks: *			denotes broken, deformed, disturbed or small sample												Prepared by JAT Date 8/29/77 Checked by _____ Date _____	

WESTENHOFF & NOVICK INC.		SUMMARY OF SOIL TEST RESULTS												Project North Side Sewage Treatment Job No. 2003 Boring No. FEC-1 Page No. 2 of 2		
ST-10	26.0-27.7				11.1	126.3									Gr f-c SAND, little f-m Gravel, little silt, trace Clay.	
SS-11	28.5-30.0	9	1.39	1.1	21.5	113.0									Same as SS-7 (more Sand).	
Remarks: *			denotes broken, deformed, disturbed or small sample												Prepared by JAT Date 8/29/77 Checked by _____ Date _____	

WESTENHOFF & NOVICK INC.		SUMMARY OF SOIL TEST RESULTS												Project North Side Sewage Treatment Job No. 2003 Boring No. FEC-2 Page No. 1 of 2		
SS-1	1.0-2.5	19			12.0										Yel-Br & Gr Silty CLAY, little f-c Sand, trace f Gravel; roots, organic material and silt pockets noted.	
SS-2	3.5-5.0	14	4.73	4.5	16.6	114.8									Dk Gr, Yel-Br & blk Silty CLAY, little f-c Sand, trace f-m Gravel; cinders and hair roots noted.	
ST-3	6.0-7.0		1.20		2.6	113.8									Br-Gr mottled blk Silty CLAY, little f-c Sand, trace f Gravel; Sand seams & roots noted.	
SS-4	8.5-10.0	9			16.9										Gr mottled Yel-Br Silty CLAY, little f-c Sand, trace f Gravel; thin silt seams and roots noted.	
ST-5	12.0-12.7		.43		.4	101.8									Dk Gr, Yel-Br & Br-Gr Silty CLAY, little f-c Sand, trace f Gravel; 2 coarse pieces of Gravel noted, wood pieces noted.	
SS-6	13.5-15.0	7	2.40	2.7	20.0	109.4									Gr Silty CLAY with thin blk Silty CLAY layers, little f-c Sand, trace f Gravel; 1" layer of Yel-Br Silty Clay, trace f-m Sand at end.	
ST-7	16.0-16.9		0.78		1.2	106.4									Yel-Br mottled blk Silty CLAY, little f-c Sand, trace f-m Gravel; organic material, roots and wood pieces noted.	
Remarks: *			denotes broken, deformed, disturbed or small sample												Prepared by JAT Date 8/29/77 Checked by _____ Date _____	

FEC-2b

WESTENHOFF & NOVICK INC.		SUMMARY OF SOIL TEST RESULTS												Project North Side Sewage Treatment Job No. 2003 Boring No. FEC-2 Page No. 2 of 2		
SS-8	18.5-20.0	39			10.1										Reddish-Yel-Br f-c SAND, some f Gravel; blk Silty Clay lenses noted.	
ST-9	22.7-23.5		0.45		0.4	23.8	105.1	31.9	15.4						Gr Silty CLAY, little f-c Sand, trace f Gravel; pink Silty Clay pockets noted.	
SS-10	23.5-25.0	4			22.5										Same as ST-9.	
ST-11	27.7-28.5		0.46		0.3	24.6	104.8								Same as ST-9 (1/2" silt layers noted).	
SS-12	28.5-30.0	5	2.20	2.1	18.2	119.4									Same as SS-10.	
Remarks: *			denotes broken, deformed, disturbed or small sample												Prepared by JAT Date 8/29/77 Checked by _____ Date _____	

WESTENHOFF & NOVICK INC.		SUMMARY OF SOIL TEST RESULTS												Project North Side Sewage Treatment Job No. 2003 Boring No. FEC-3 Page No. 1 of 2		
SS-1	1.0-2.5	9	6.36	4.5	12.7	117.8	32.4	15.8							Yel-Br & Gr slightly mottled Silty CLAY, little f-c Sand, trace f Gravel; thin silt seams and pockets noted.	
ST-2	6.0-6.3-6.3-7.0		0.72		1.1	26.0	99.4	50.5	19.9	36.7	16.7				Gr mottled Yel-Br & Dk Gr Silty CLAY, little f-c Sand, trace f-m Gravel; thin blk Silty Clay seams noted-top 3" Gr mottled Br & Dk Gr Silty CLAY, trace f-m Sand.	
SS-3	8.5-10.0	7	4.89	4.5	27.4	98.7	57.2	20.9							Gr mottled Yel-Br Silty CLAY, trace f-m Sand.	
ST-4	11.0-12.7		0.65		2.1	27.1	33.5	15.9							11-11.7 Gr & Yel-Br mottled Silty CLAY, trace f-c Sand, trace f Gravel. 11.7-12.7 Gr mottled Yel-Br changing to Gr Clayey SILT, some f-c Sand, trace f-m Gravel; Sand seams noted and Silty Clay layers noted.	
SS-5	13.5-15.0	7	1.78	1.7	16.0	119.1									Gr Clayey SILT, little f-c Sand, trace f Gravel; Silty Clay and Sand layers noted.	
ST-6	17.7-18.5		0.45		0.5	21.1	107.6								Gr Silty CLAY, little f-c Sand, trace f Gravel.	
Remarks: *			denotes broken, deformed, disturbed or small sample												Prepared by JAT Date 8/29/77 Checked by _____ Date _____	

WESTENHOFF & NOVICK INC.		SUMMARY OF SOIL TEST RESULTS												Project North Side Sewage Treatment Job No. 2003 Boring No. FEC-3 Page No. 2 of 2		
SS-7	18.5-20.0	4	0.73	0.7	21.7	108.5									Same as ST-6.	
ST-8	22.7-23.0		0.43		0.3	26.3	101.5	33.0	15.9						Same as ST-6 (pink Silty Clay pockets noted).	
SS-9	23.5-25.0	4	0.73	0.5	21.6	110.2									Same as SS-7.	
ST-10	27.7-28.5		0.87		1.0	21.0	112.7								Same as SS-7 (medium Gravel noted).	
SS-11	28.5-30.0	5	1.94	1.4	18.4	107.1									Same as SS-7 (more Sand).	
Remarks: *			denotes broken, deformed, disturbed or small sample												Prepared by JAT Date 8/29/77 Checked by _____ Date _____	

RETA ENGINEERS / A JOINT VENTURE CHICAGO

REVISIONS		
NO	DATE	BY

THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO

NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 78-020-CP SECONDARY TREATMENT FACILITIES

LABORATORY TEST DATA

Correct _____

Approved _____ Assistant Chief Engineer

Approved _____ Chief Engineer

SCALES SHOWN ARE SCALES OF TRACINGS

Designed D.W. Draw _____ Checked R.W.B. Reviewed _____ DATE APR 1988 SHEET NO 2C-72

TFB-1

WESTENHOFF & NOVICK INC. CHICAGO, ILLINOIS SUMMARY OF SOIL TEST RESULTS Project North Side Sewage Treatment Job No. 2001 Boring No. TFB-1 Page No. 1 of 3

WESTENHOFF & NOVICK INC. CHICAGO, ILLINOIS SUMMARY OF SOIL TEST RESULTS Project North Side Sewage Treatment Job No. 2001 Boring No. TFB-1 Page No. 2 of 3

WESTENHOFF & NOVICK INC. CHICAGO, ILLINOIS SUMMARY OF SOIL TEST RESULTS Project North Side Sewage Treatment Job No. 2001 Boring No. TFB-1 Page No. 3 of 3

WESTENHOFF & NOVICK INC. CHICAGO, ILLINOIS SUMMARY OF SOIL TEST RESULTS Project North Side Sewage Treatment Job No. 2001 Boring No. TFB-2 Page No. 1 of 2

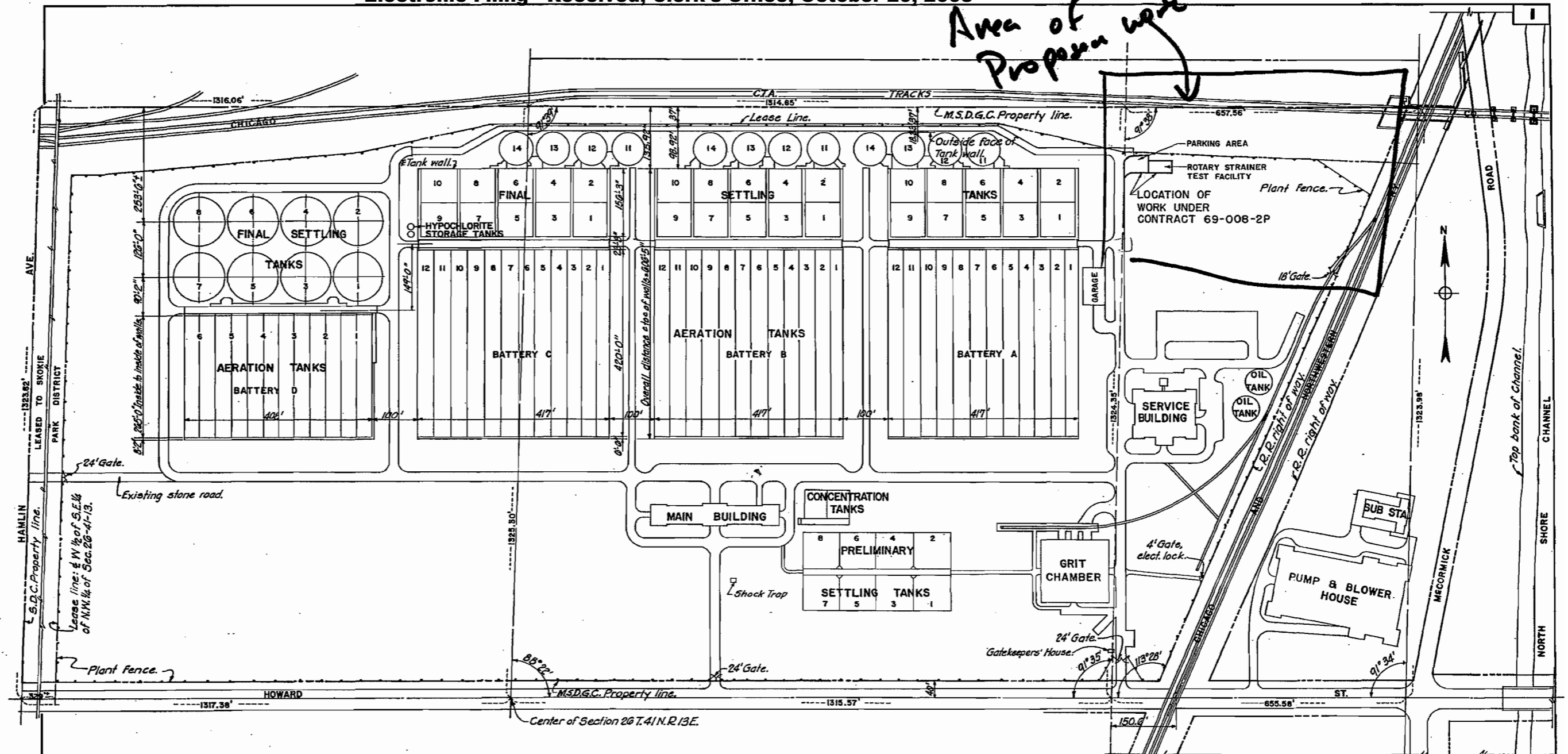
WESTENHOFF & NOVICK INC. CHICAGO, ILLINOIS SUMMARY OF SOIL TEST RESULTS Project North Side Sewage Treatment Job No. 2001 Boring No. TFB-2 Page No. 2 of 2

REVISIONS table with columns NO, DATE, BY

THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 78-020-CP SECONDARY TREATMENT FACILITIES LABORATORY TEST DATA

Approval signatures and dates: Correct, Approved, Assistant Chief Engineer, Chief Engineer, SCALES SHOWN ARE SCALES OF TRACINGS, DATE: APR, 1986 SHEET NO 2C-94

Area of Proposed work

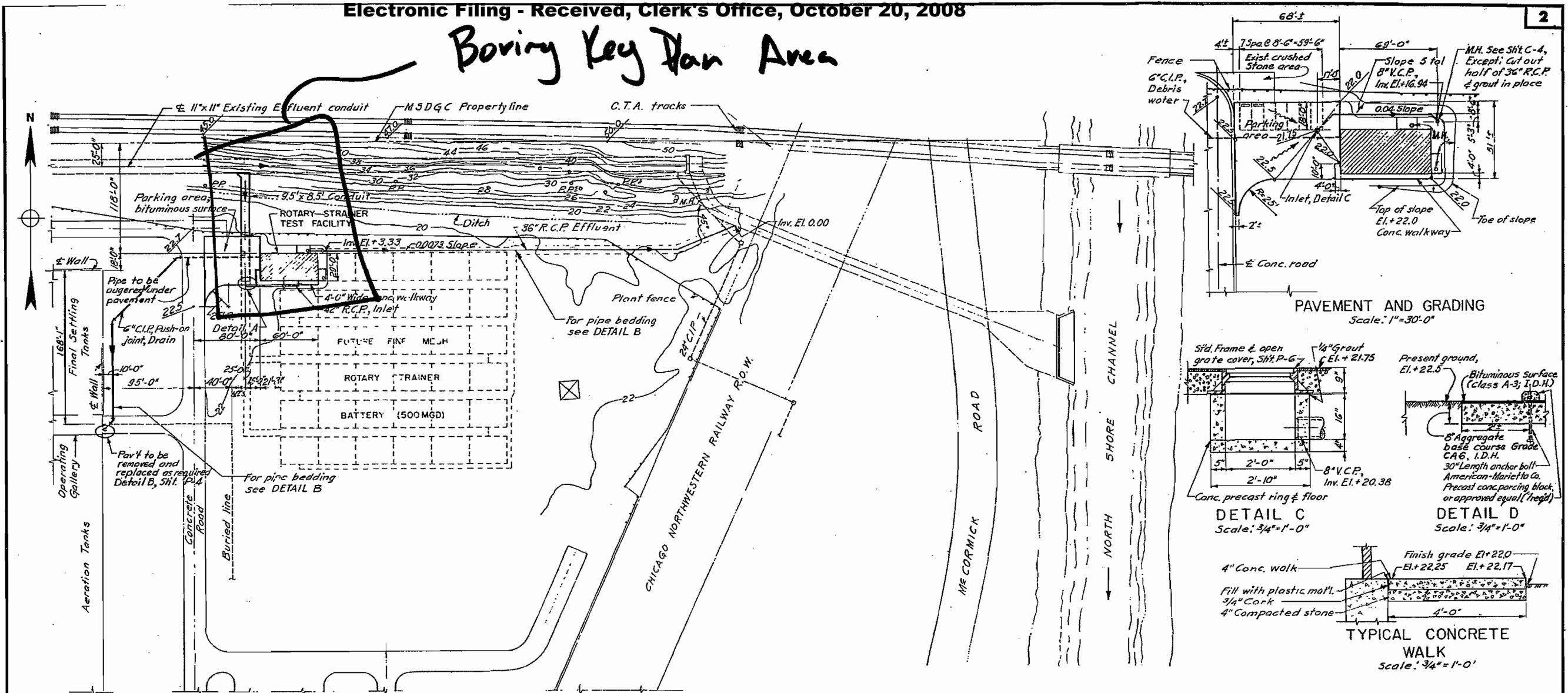


LEGEND:
 — Work under Contract 69-008-2P
 — Existing structures, roads, etc.

REVISIONS			THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO	John Varialogis Robert Barbini Ben Szwed Frank Wood
NO.	DATE	BY		
			NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 69-008-2P SITE PREPARATION FOR FINE MESH ROTARY STRAINER LOCATION PLAN	SCALES SHOWN ARE SCALES OF TRACINGS

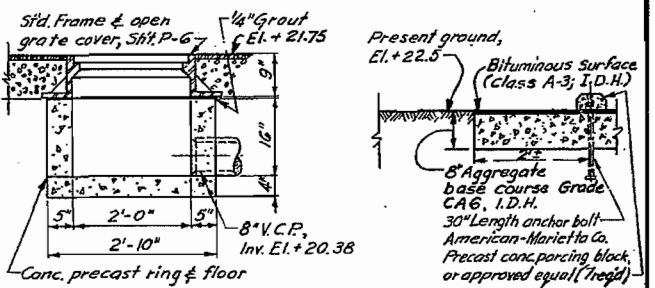
DATE NOV., 1969 SHEET NO. P-1

Boring Key Van Area

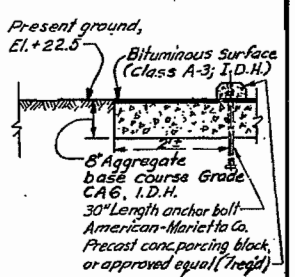


PLAN
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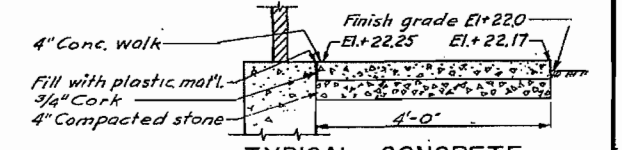
PAVEMENT AND GRADING
Scale: 1"=30'-0"



DETAIL C
Scale: 3/4"=1'-0"

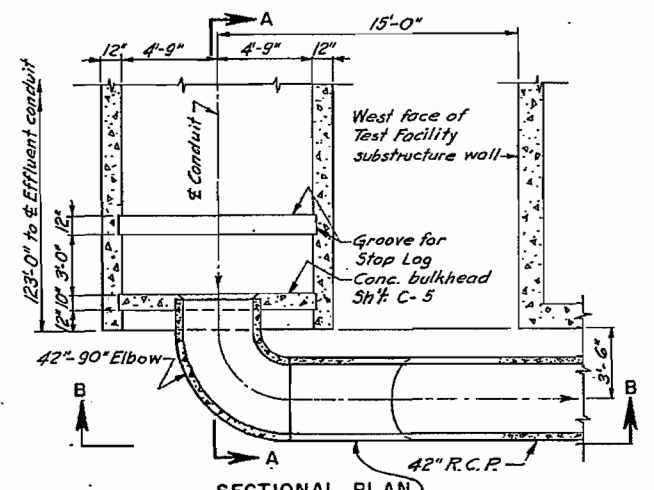


DETAIL D
Scale: 3/4"=1'-0"

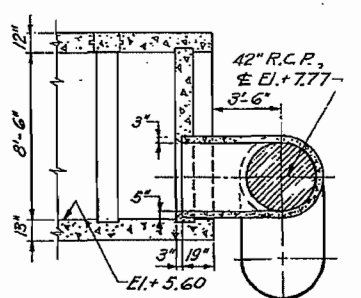


TYPICAL CONCRETE WALK
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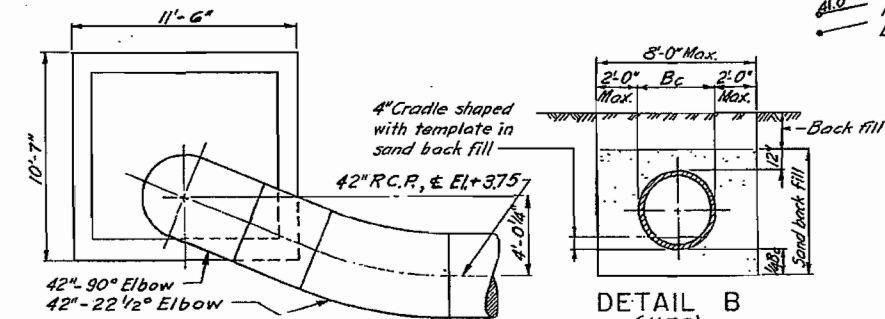
LEGEND:
 • PP Power pole
 Δ Proposed Elevation
 — Existing Elevation



SECTIONAL PLAN
Provide concrete thrust blocks



SECTION A-A



SECTION B-B

DETAIL B
(N.T.S)
Trench-pipe bedding

DETAIL A
Scale: 1/4"=1'-0"

REVISIONS		
NO.	DATE	BY

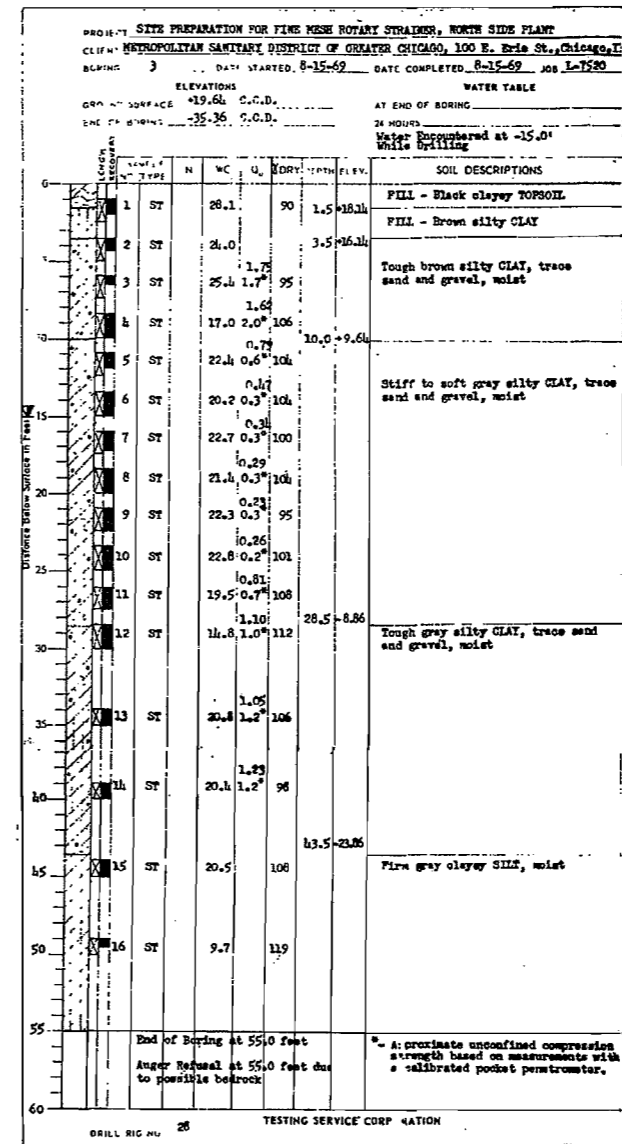
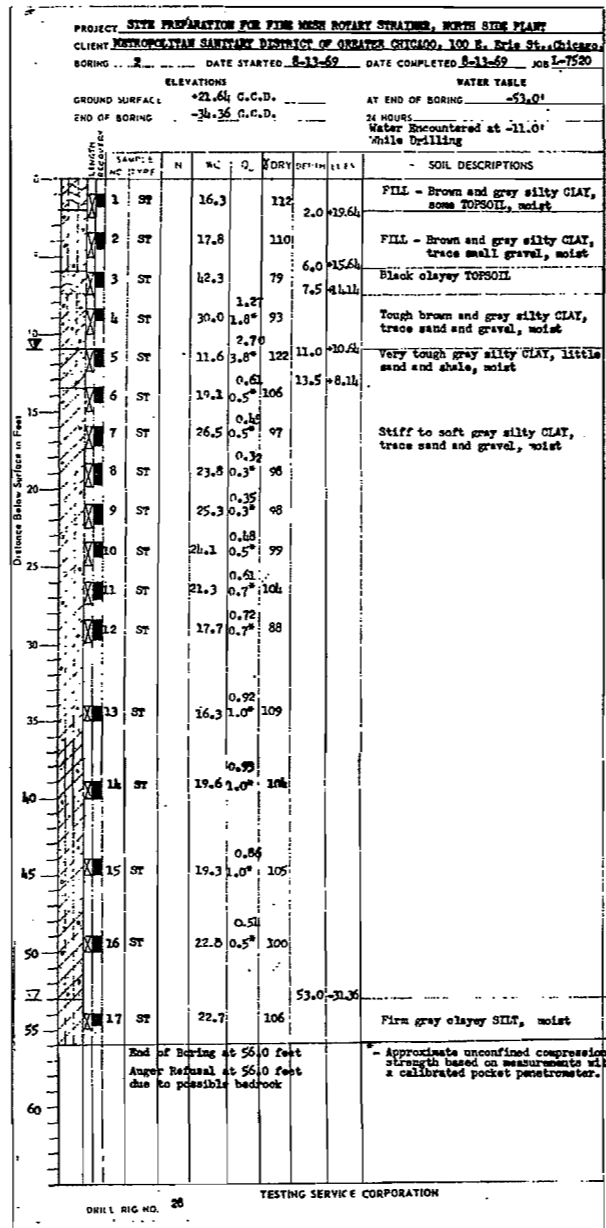
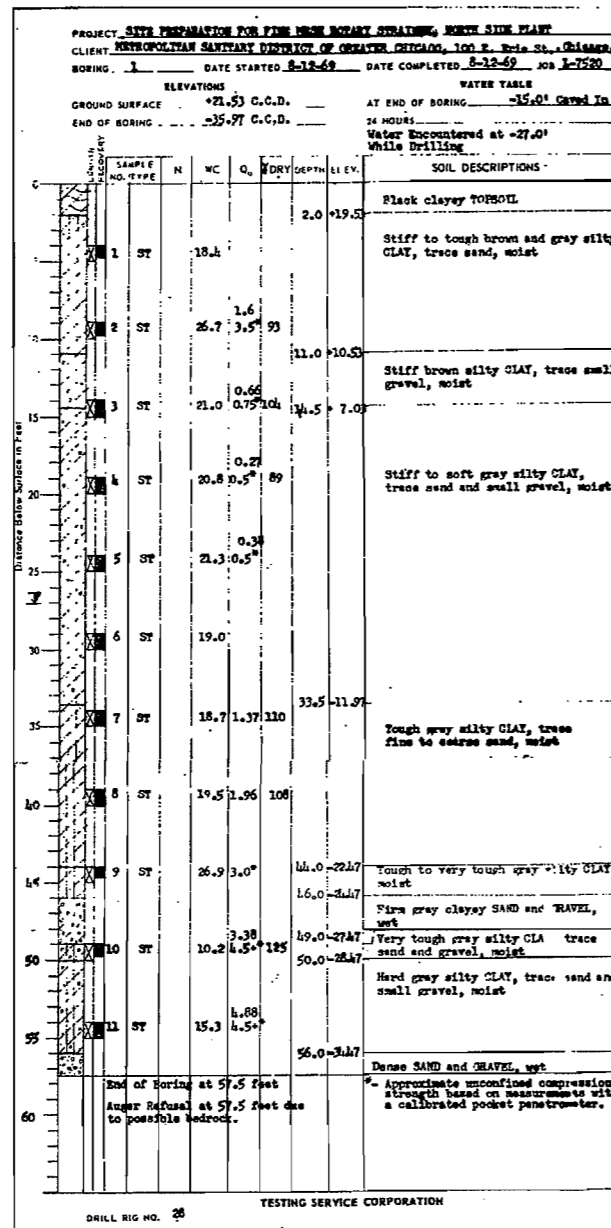
THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO
NORTH SIDE SEWAGE TREATMENT WORKS
CONTRACT 69-008-2P
 SITE PREPARATION FOR FINE MESH ROTARY STRAINER
GENERAL PLAN AND TOPOGRAPHY
DETAILS

Drawn: H.T. Checked: F.K. Examined: M.H. DATE: NOV, 1969

John Variakojis
 Robert Balchini
 Asst. Asst. Eng.
 Fred W. ...

SCALES SHOWN ARE SCALES OF TRACINGS

SHEET NO. P-2



GENERAL NOTES

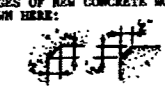
DETAILS AND NOTES RELATIVE TO EXISTING WORK ARE REASONABLY CORRECT BUT ARE NOT GUARANTEED BY THE SANITARY DISTRICT.

THE CONTRACTOR SHALL CHECK ALL DETAILS, ELEVATIONS, AND MATERIALS IN THE FIELD AND SHALL ARRANGE THE NEW WORK TO SUIT, ALL AS APPROVED BY THE ENGINEER. THE COST OF SUCH WORK SHALL BE INCLUDED IN THE UNIT AND LUMP SUM PRICES FOR THE VARIOUS ITEMS.

THE SOIL BORING INFORMATION IS BELIEVED TO BE ACCURATE BUT IS NOT GUARANTEED BY THE SANITARY DISTRICT. THE CONTRACTOR MUST SATISFY HIMSELF BY MAKING BORINGS OR BY ANY OTHER METHOD AS HE MAY PREFER, AS TO THE CHARACTER OF SOILS AND THE AMOUNT OF WATER, BOULDERS, ROCK AND OTHER MATERIALS HE MAY ENCOUNTER IN THE WORK TO BE PERFORMED UNDER THIS CONTRACT.

ALL EXCAVATION SHALL BE PERFORMED WITHIN THE NARROWEST PRACTICAL LIMITS SO THAT THE LOAD CARRYING CAPACITY OF THE SOIL UNDER ANY NEARBY FOOTING WILL NOT, IN THE OPINION OF THE ENGINEER, BE UNNECESSARILY DECREASED.

ALL EXPOSED EDGES OF NEW CONCRETE WORK SHALL HAVE A 1/2-INCH CHAMFER AS SHOWN HERE:



THE FOLLOWING ABBREVIATIONS ARE USED IN LOCATING REINFORCEMENT BARS: "BT" DEMOTES BOTTOM; "BT" DEMOTES TOP; "T.F." DEMOTES REAR FACE; "F.F." DEMOTES FAR FACE; "E.F." DEMOTES EACH FACE.

MAIN REINFORCEMENT BARS IN THE TOP AND BOTTOM OF SLABS NOT IN CONTACT WITH SOIL SHALL HAVE A 1-INCH CLEAR COVERING OF CONCRETE FROM THE FACES TO WHICH THEY ARE ADJACENT, EXCEPT AS NOTED.

MAIN REINFORCEMENT BARS IN SLABS IN CONTACT WITH SOIL SHALL HAVE A 3-INCH CLEAR COVERING OF CONCRETE.

MAIN REINFORCEMENT BARS IN WALLS SHALL HAVE A 2-INCH CLEAR COVERING OF CONCRETE.

REINFORCING BARS AT OPENINGS SMALLER THAN 12-INCH DIAMETER SHALL BE REARRANGED IN FIELD TO SUIT, AS APPROVED BY THE ENGINEER.

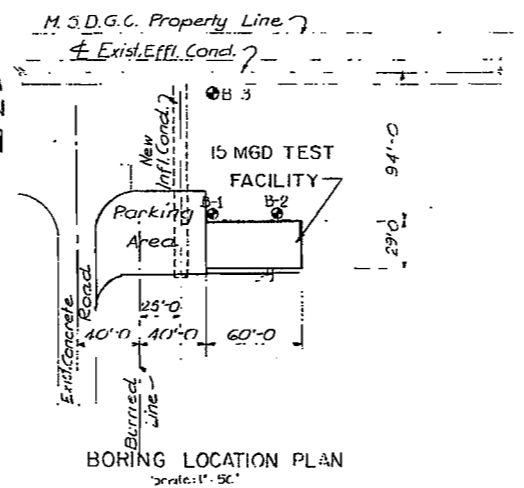
PIPE SLEEVES, FRAMES, ANCHOR BOLTS, INSERTS, ETC., SHALL BE SET IN PLACE BEFORE CONCRETE IS POURED. THE CONTRACTOR IS REQUIRED TO CHECK ALL DRAWINGS AND SHOP DETAILS OF EQUIPMENT AND PREFABRICATED HOUSING FOR THE SIZE AND LOCATION OF ALL INSERTS.

IN REMOVING EXISTING CONCRETE AND MASONRY, PROPER PRECAUTION SHALL BE TAKEN TO PREVENT THE SPALLING OF THE CONCRETE AND MASONRY BEYOND THE CUTTING LINES. ANY PATCHING REQUIRED SHALL BE DONE AS DIRECTED BY THE ENGINEER AND SHALL BE AT THE CONTRACTOR'S EXPENSE.

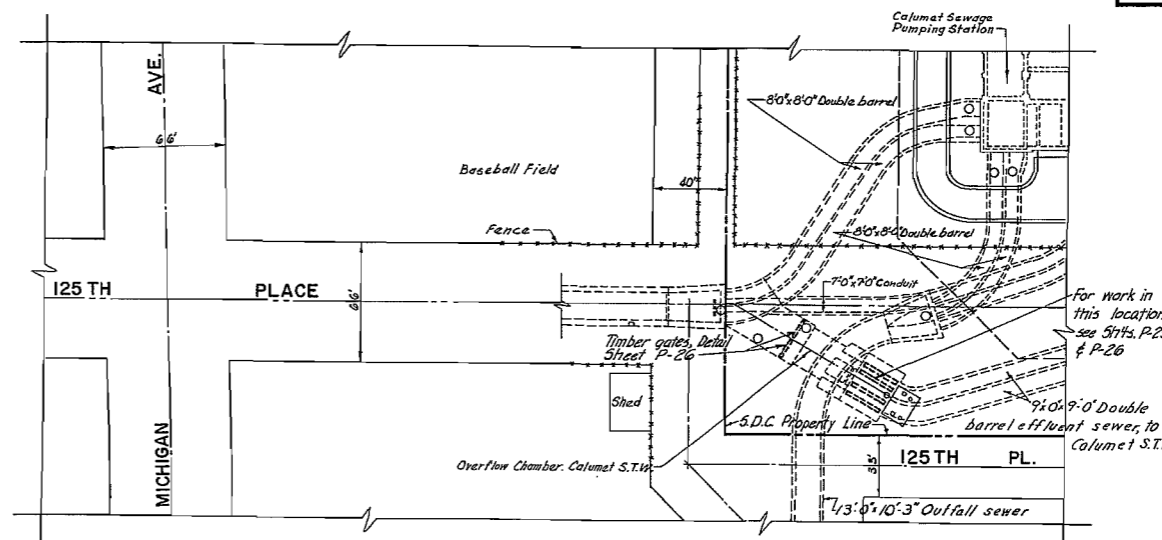
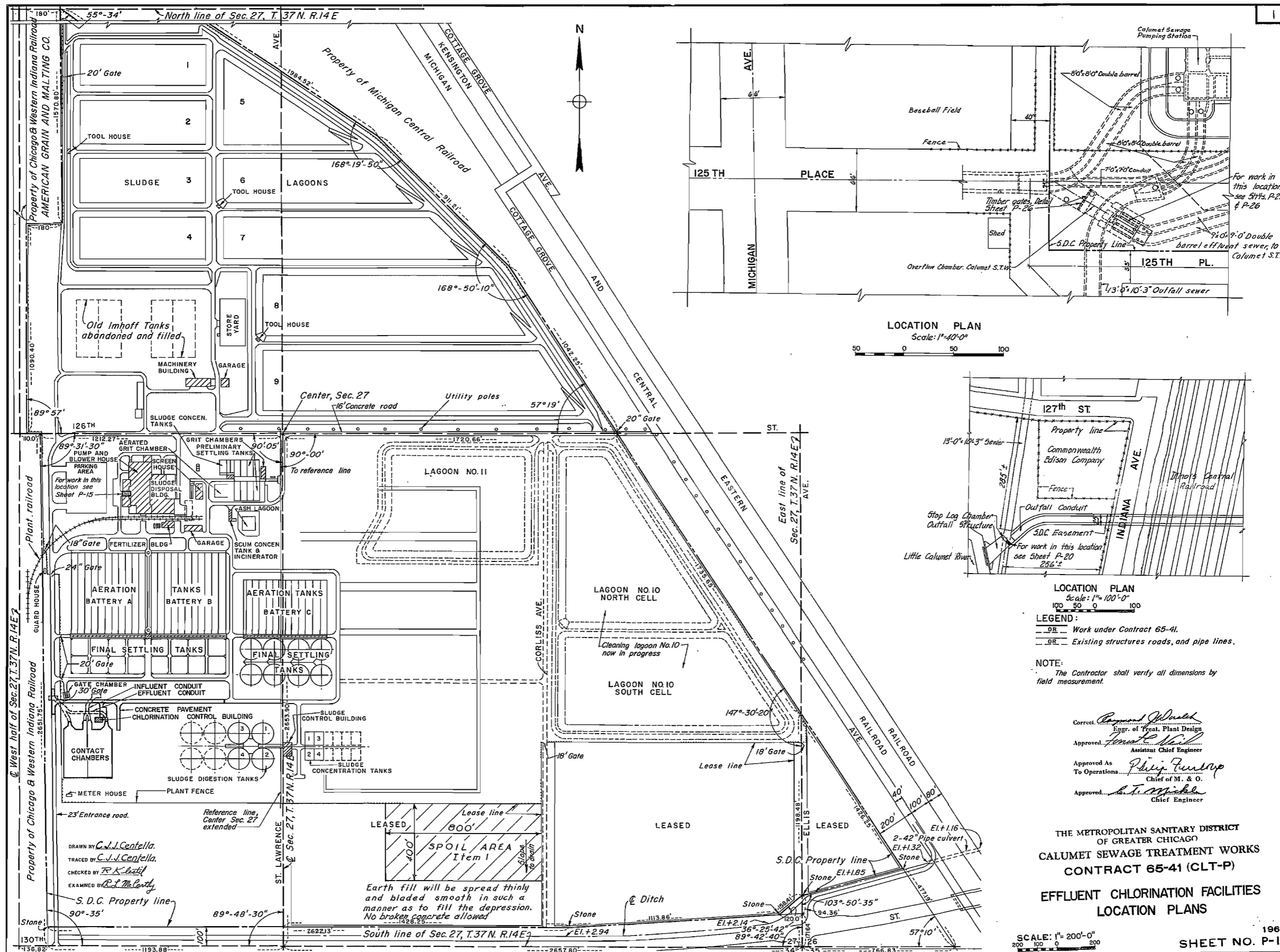
WHERE NEW CONCRETE IS TO COVER EXISTING CONCRETE SURFACES, SUCH SURFACES SHALL BE THOROUGHLY CLEANED AND LEFT ROUGH TO INSURE GOOD CONTACT BETWEEN THE OLD AND THE NEW CONCRETE.

THROUGHOUT THIS SET OF DRAWINGS EXISTING STRUCTURES ARE SHOWN IN LIGHT LINES; NEW AND ALTERED WORK IS SHOWN IN HEAVY OUTLINES.

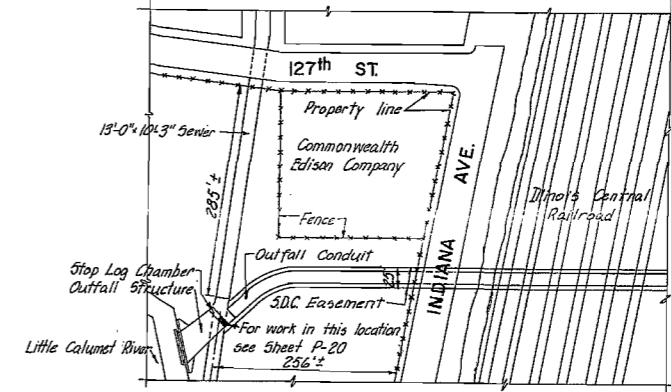
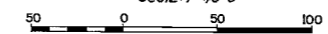
ALL CROSS HATCHED AREAS BOUNDED BY HEAVY FULL LINES INDICATE MATERIALS TO BE REMOVED.



REVISIONS			THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO	
NO.	DATE	BY		
			NORTH SIDE SEWAGE TREATMENT WORKS CONTRACT 69-008-2P SITE PREPARATION FOR FINE MESH ROTARY STRAINER SOIL BORING LOG	
			Correct <i>Leslie Sombra</i> Engineer of Structural Design Approved <i>Robert Barabian</i> Assistant Chief Engineer Approved As To Operations <i>Dr. Smoot</i> Acting Chief of M. & O. Approved <i>Frank K. Hill</i> Acting Chief Engineer SCALES SHOWN ARE SCALES OF TRACINGS	
Drawn <i>E. Cozike</i> Traced Checked <i>L.P. NAWK</i>			DATE NOV., 1969	SHEET NO. C-1



LOCATION PLAN
Scale: 1"=40'-0"



LOCATION PLAN
Scale: 1"=100'-0"

- LEGEND:
- Work under Contract 65-41.
 - Existing structures, roads, and pipe lines.

NOTE:
The Contractor shall verify all dimensions by field measurement.

Corrected: *Raymond J. Smith*
Engr. of Treat. Plant Design
Approved: *Frankie Hill*
Assistant Chief Engineer
Approved As To Operations: *Philip F. Fursup*
Chief of M. & O.
Approved: *A. T. Cappella*
Chief Engineer

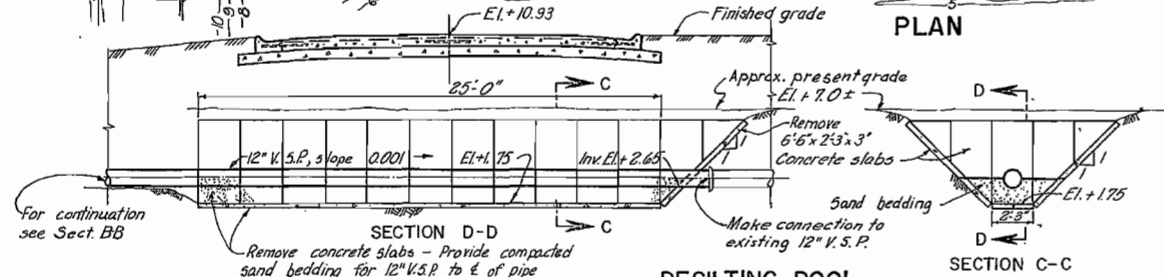
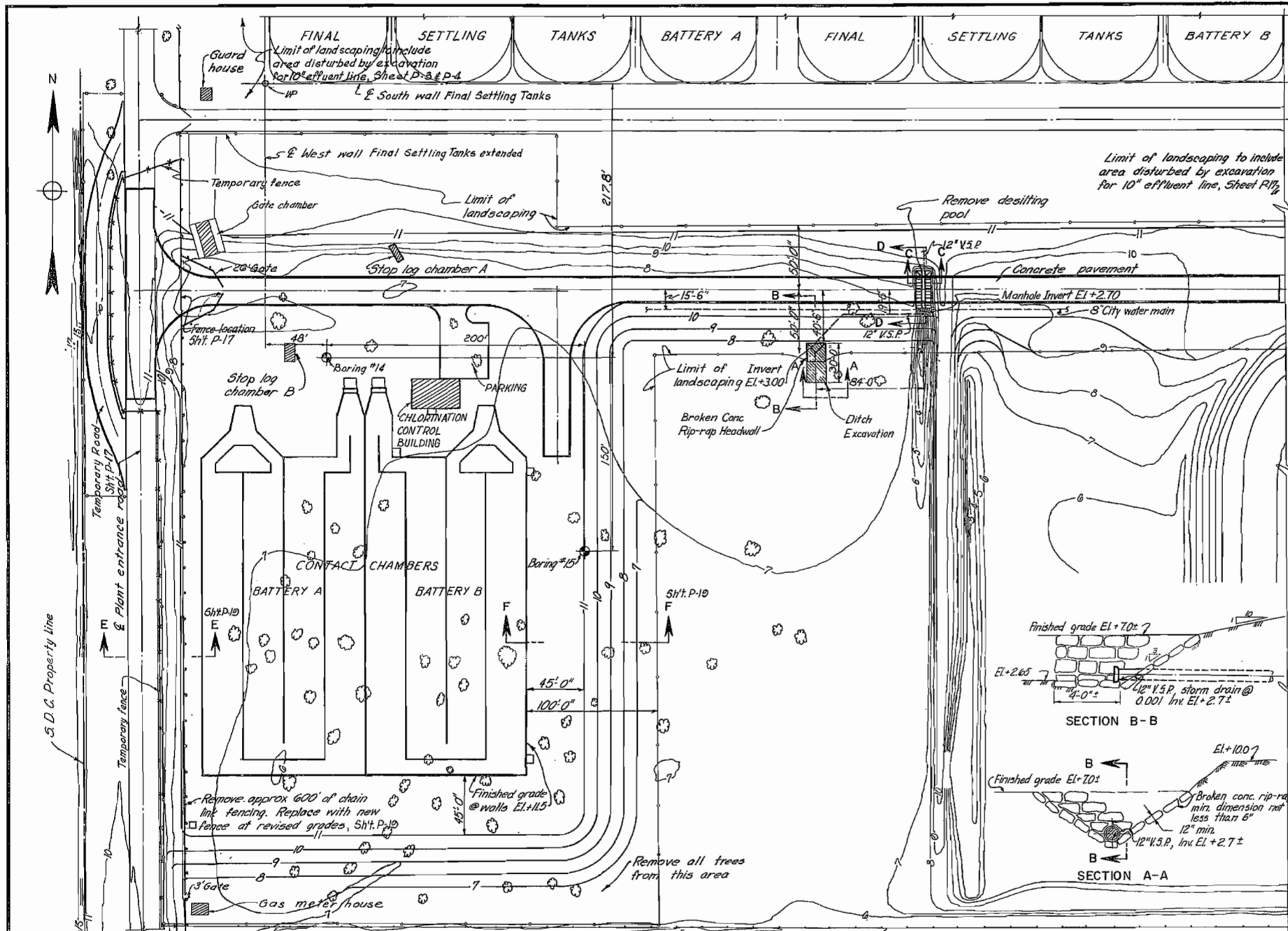
THE METROPOLITAN SANITARY DISTRICT
OF GREATER CHICAGO
CALUMET SEWAGE TREATMENT WORKS
CONTRACT 65-41 (CLT-P)
EFFLUENT CHLORINATION FACILITIES
LOCATION PLANS

SCALE: 1"=200'-0"
200 100 0 200
1966
SHEET NO. P-1

DRAWN BY: *C. J. Centella*
TRACED BY: *C. J. Centella*
CHECKED BY: *R. K. Bost*
EXAMINED BY: *R. L. McCarty*

S.D.C. Property line
90'-35'

130TH ST



LEGEND

- Work under Contract 65-41
- Existing structures, roads, etc.
- Limits of landscaping, Item 1
- Trees

NOTE

All trees and debris within the work area and south to plant fence shall be removed and disposed by the Contractor. Some trees are over 6" in diameter. Location and number shown are approximate and not guaranteed. The Contractor shall verify number and size to be removed. Trees which do not interfere with work under this contract shall be preserved if ordered by the Engineer. Removal shall include stumps. Item 1.

REVISIONS	
Date: June 22, 1967, Letter File No. 129	Broken concrete rip-rap headwall relocated.

DRAWN BY: *M.U. & K.W.G.*
 TRACED BY: *R.L. Hestel*
 CHECKED BY: *R.L. Hestel*
 EXAMINED BY: *R.L. Hestel*

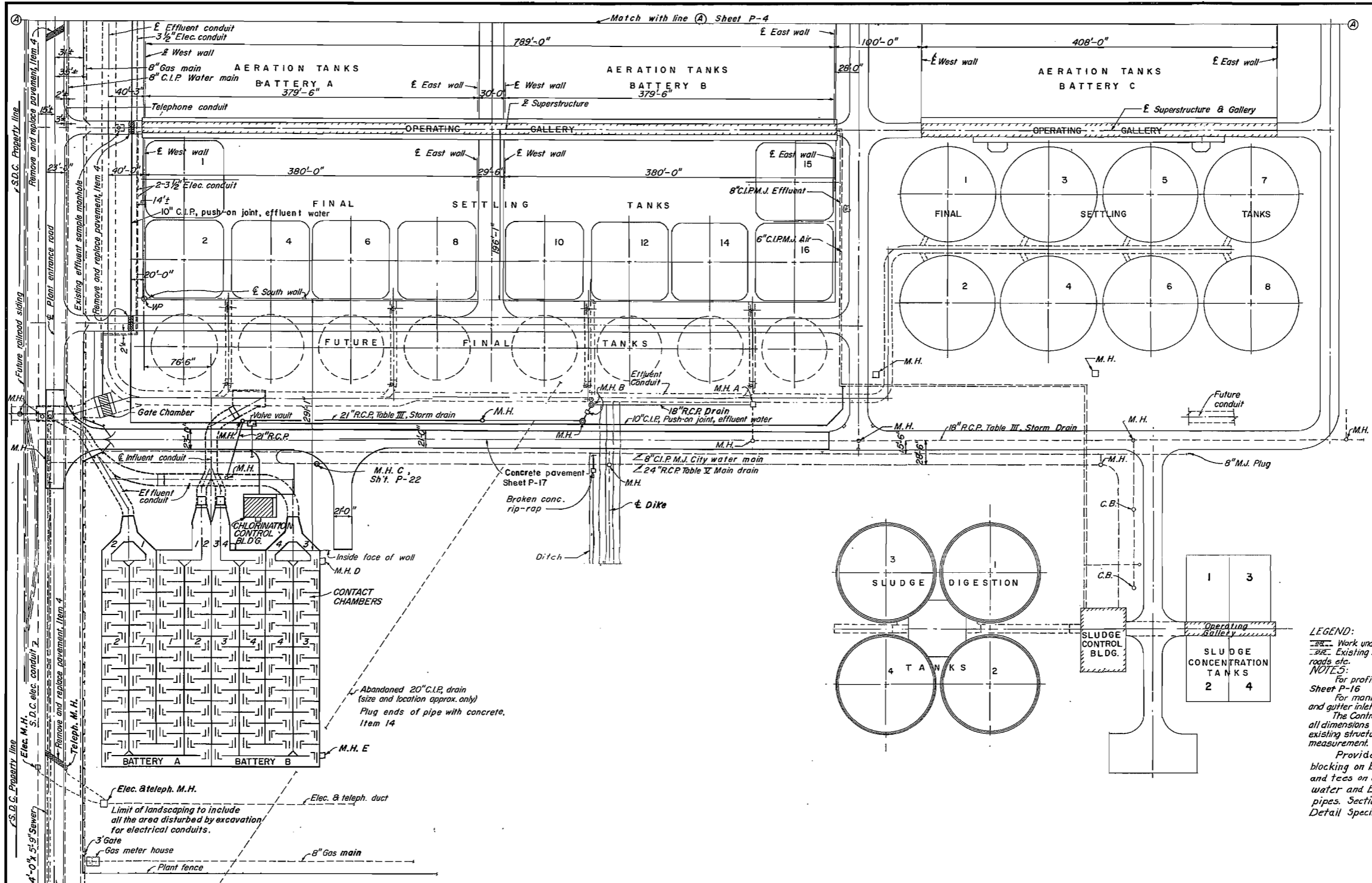
LOG OF BORING NO. 14			
OWNER METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO		ARCHITECT-ENGINEER	
SITE 125th and Indiana - Chicago		PROJECT NAME CALUMET SEWAGE TREATMENT WORKS EXPANSION	
DEPTH	DESCRIPTION OF MATERIAL	DEPTH	LOG
1 ST	NOTE A	109	
2 ST	SILTY CLAY; TRACE SAND AND GRAVEL; BROWN & GRAY; VERY TOUGH; (CL)	109	
3 ST		110	
4 ST	SILTY CLAY; TRACE SAND AND GRAVEL; GRAY; VERY TOUGH TO HARD; (CL)	110	
5 ST		121	
6 ST		107	
7 ST		122	
8 ST		120	
9 ST		121	
10 ST		124	
11 ST		127	

LOG OF BORING NO. 15			
OWNER METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO		ARCHITECT-ENGINEER	
SITE 125th and Indiana - Chicago		PROJECT NAME CALUMET SEWAGE TREATMENT WORKS EXPANSION	
DEPTH	DESCRIPTION OF MATERIAL	DEPTH	LOG
1 ST	NOTE A	108	
2 ST	SILTY CLAY; TRACE SAND; GRAY, BROWN & GRAY; HARD; (CL)	94	
3 ST		114	
4 ST	SILTY CLAY; TRACE SAND; GRAY & BROWN; V. TOUGH; (CL)	115	
5 ST		102	
6 ST	SILTY CLAY; SOME FINE SAND; TRACE GRAVEL WITH OCCASIONAL BEANS OF SILT; GRAY; HARD; (CL)	100	
7 ST		118	
8 ST		118	
9 ST	SILTY CLAY; SOME FINE SAND; TRACE GRAVEL WITH BEANS OF SILT & FINE SAND; GRAY; HARD; HANDPAN; (CL)	132	
10 ST		123	
11 ST	NOTE C		

THE METROPOLITAN SANITARY DISTRICT OF GREATER CHICAGO
 CALUMET SEWAGE TREATMENT WORKS
 CONTRACT 65-41 (CLT-P)
 TOPOGRAPHY
 BORINGS
 GRADING & FENCING

SCALE: 1" = 40'-0"
 SHEET NO. P-2

1228/100186



LEGEND:
 - - - - - Work under Contract 65-41
 - - - - - Existing structures, piping, roads, etc.
NOTES:
 For profile of pipe lines, Sheet P-16
 For manhole, catch basin, and gutter inlet details, Sheet P-17
 The Contractor shall verify all dimensions and elevations of existing structures by field measurement.
 Provide concrete blocking on bends, stubs and tees on cast iron, City water and Effluent water pipes. Section II7 of the Detail Specifications.

DRAWN BY M.U. & K.W.G.
 TRACED BY
 CHECKED BY M. Kelly
 EXAMINED BY R.J. McCreary

Corrected Raymond J. Walsh
 Supv. of Treat. Plant Design
 Approved Samuel J. Hill
 Assistant Chief Engineer
 Approved As To Operations Philip J. Furlong
 Chief of M. & O.
 Approved R.T. Mickle
 Chief Engineer

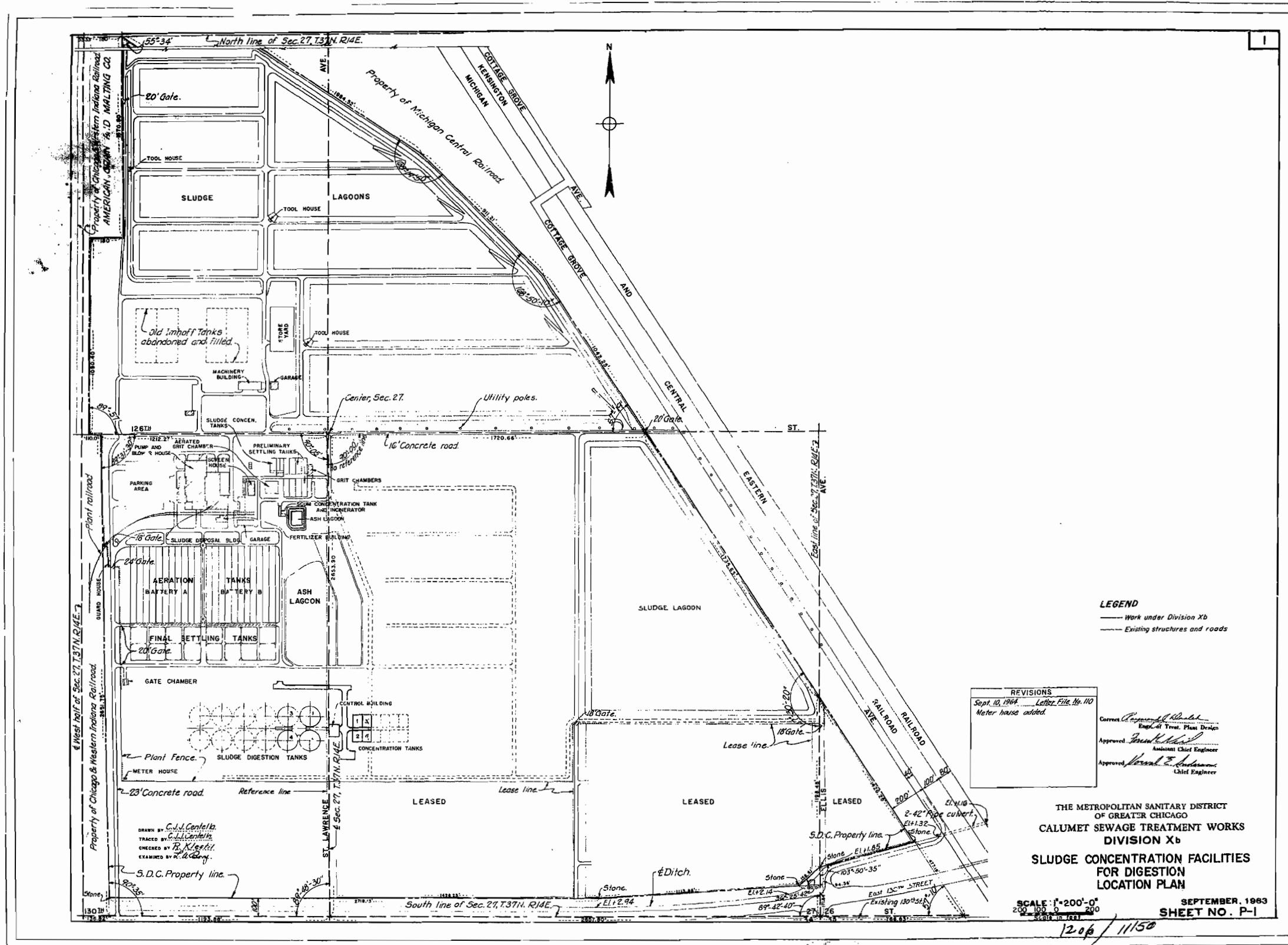
THE METROPOLITAN SANITARY DISTRICT
 OF GREATER CHICAGO
 CALUMET SEWAGE TREATMENT WORKS
 CONTRACT 65-41 (CLT-P)

GENERAL LAYOUT
 SOUTH HALF

SCALE: 1" = 50'-0"
 50 100
 Scale in feet

1966
 SHEET NO. P-3

1228/100186



LEGEND
 — Work under Division Xb
 - - - Existing structures and roads

REVISIONS	
Sept. 10, 1964	Letter File No. 110 Meter house added.

Correa *[Signature]*
 Engr. of Treat. Plant Design
 Approved *[Signature]*
 Assistant Chief Engineer
 Approved *[Signature]*
 Chief Engineer

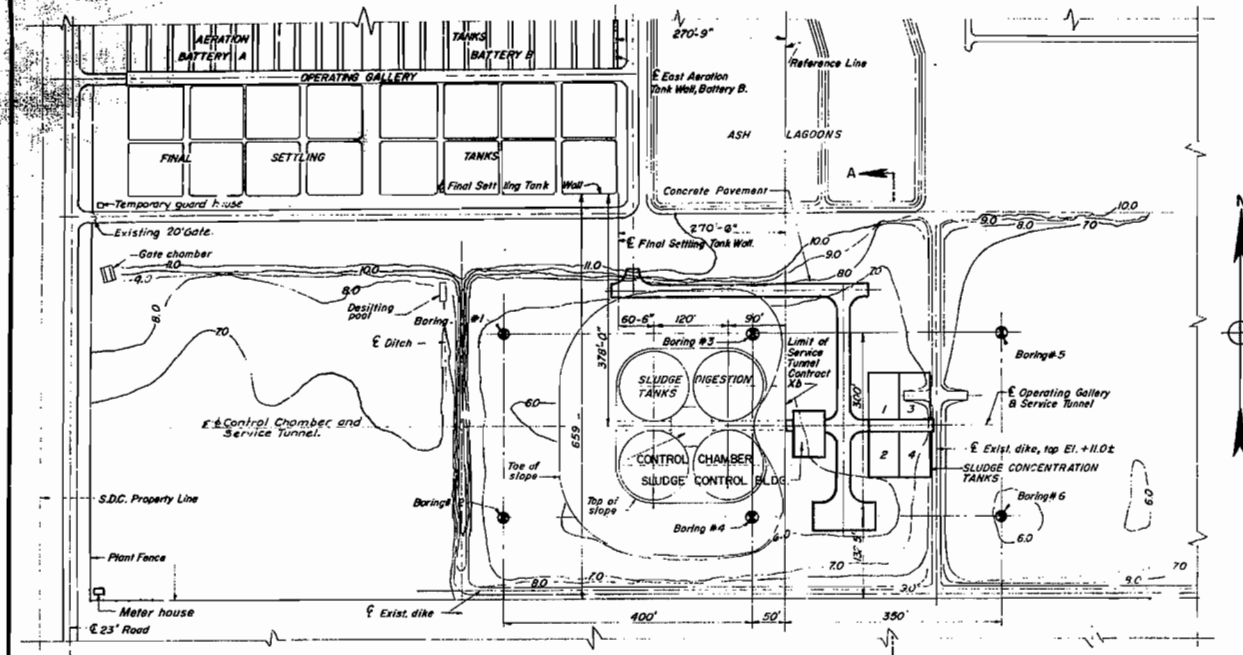
THE METROPOLITAN SANITARY DISTRICT
 OF GREATER CHICAGO
 CALUMET SEWAGE TREATMENT WORKS
 DIVISION Xb
 SLUDGE CONCENTRATION FACILITIES
 FOR DIGESTION
 LOCATION PLAN

SCALE: 1" = 200'-0"
 200' 0" 0" 200'
 1" = 200' 0"

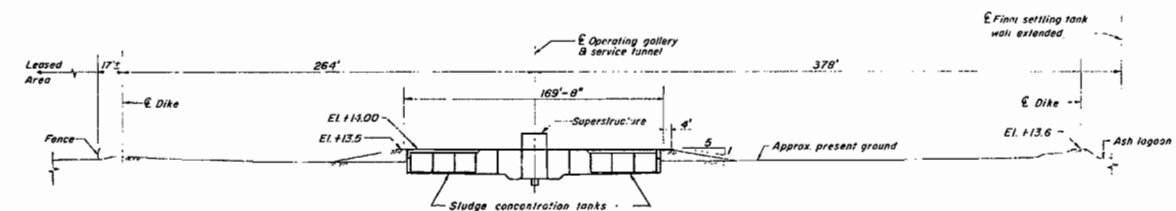
SEPTEMBER, 1963
 SHEET NO. P-1

1206/1150

DRAWN BY: C.J.J. Conella
 TRACED BY: C.J.J. Conella
 CHECKED BY: R. Klestil
 EXAMINED BY: R. G. Gung.



PLAN
Scale: 1"=100'-0"
Borings shown on Sheet No. P-3



SECTION A-A
Scale: 1"=40'-0"

LEGEND
 - - - Work under Division Xb.
 — Existing structures, roads and pipe lines.

DRAWN BY: C.W.C. & M.U.
 TRACED BY: M. Urbank
 CHECKED BY: J. H. [Signature]
 EXAMINED BY: L. H. [Signature]

REVISIONS	
Sept. 10, 1964	Letter File No. 110 Meter house added.

Corrected: Raymond J. [Signature]
 Engr. of Treat. Plant Design
 Approved: [Signature]
 Assistant Chief Engineer
 Approved: [Signature]
 Chief Engineer

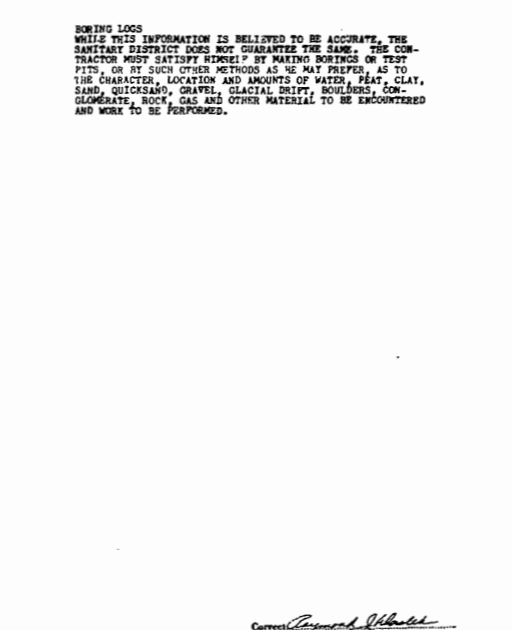
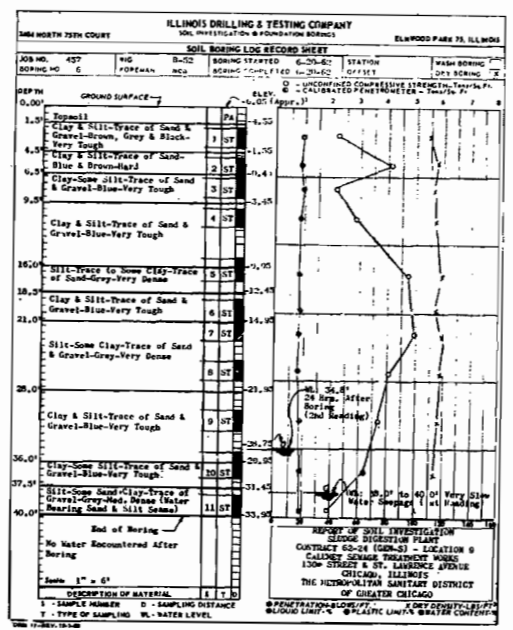
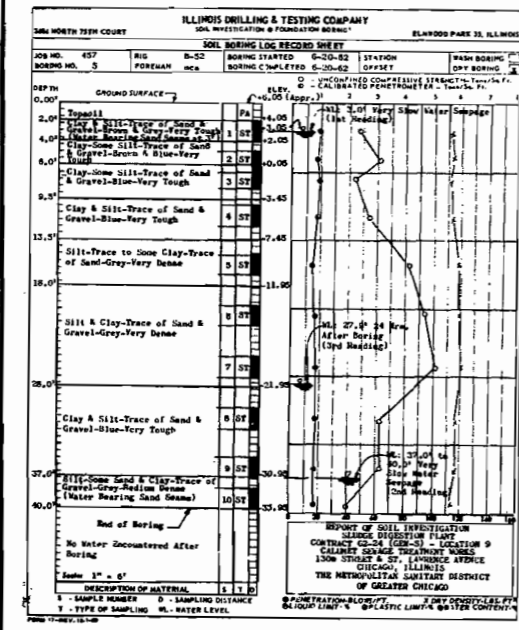
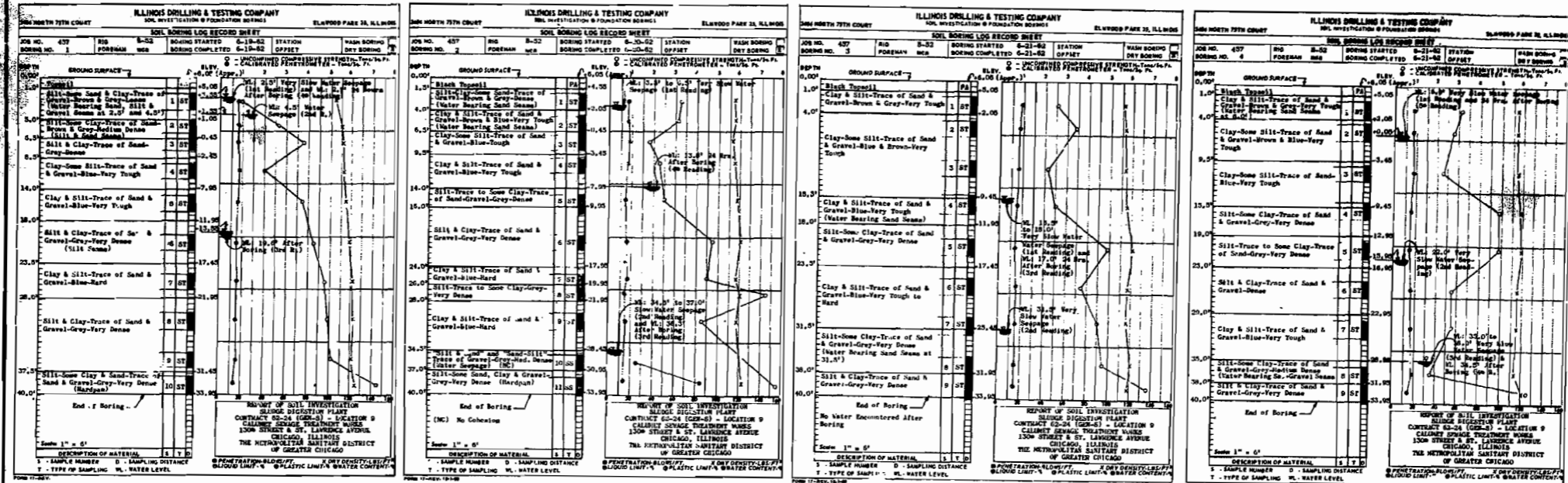
THE METROPOLITAN SANITARY DISTRICT
 OF GREATER CHICAGO
 CALUMET SEWAGE TREATMENT WORKS
 DIVISION Xb

TOPOGRAPHY

SCALE: AS SHOWN

SEPTEMBER, 1963
 SHEET NO. P-2

1206/1150

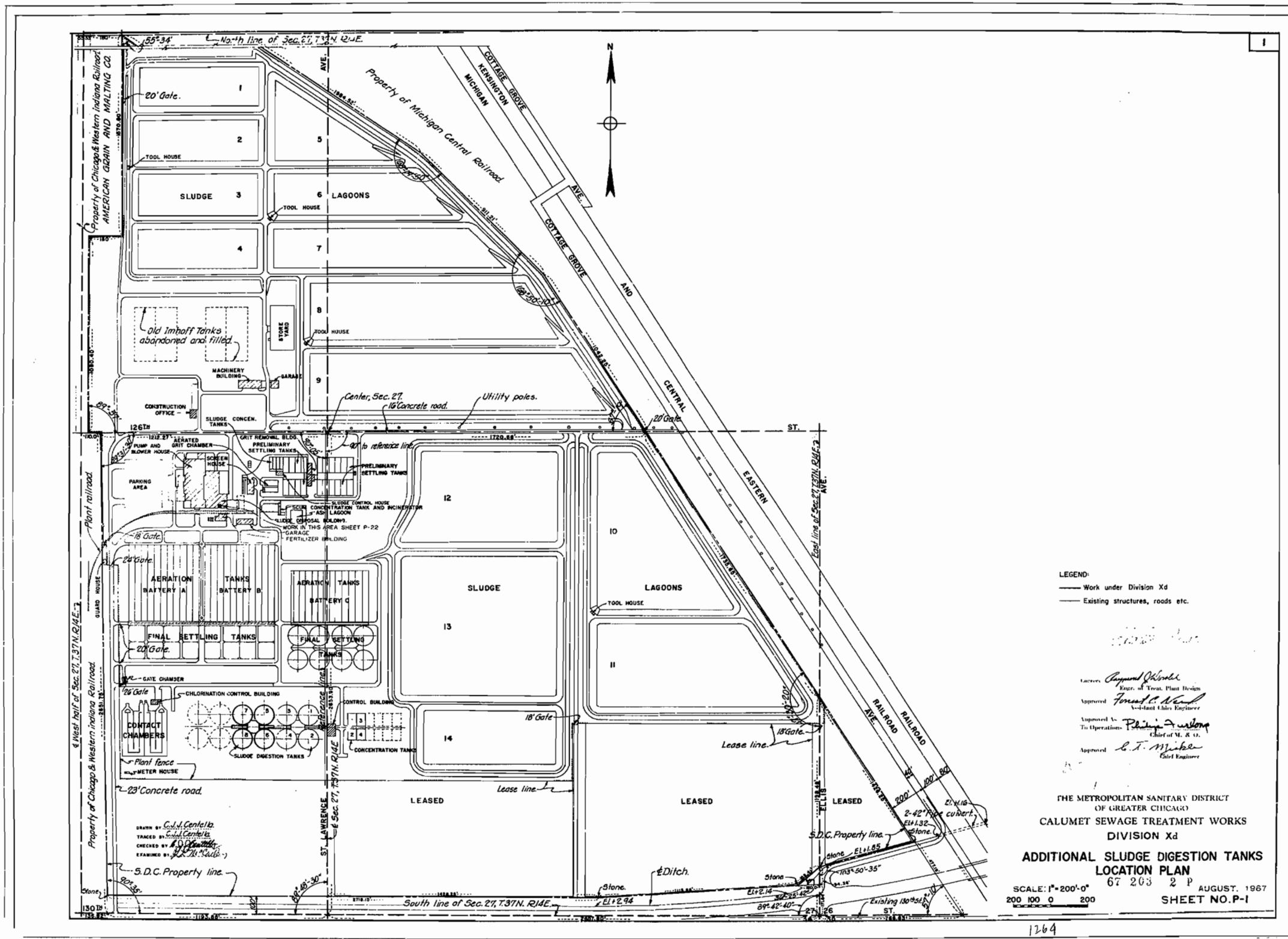


BORING LOGS
WHILE THIS INFORMATION IS BELIEVED TO BE ACCURATE, THE SANITARY DISTRICT DOES NOT GUARANTEE THE SAME. THE CONTRACTOR MUST SATISFY HIMSELF BY MAKING BORINGS OR TEST PITS, OR BY SUCH OTHER METHOD AS HE MAY PREFER, AS TO THE CHARACTER, LOCATION AND AMOUNTS OF WATER, PEAT, CLAY, SAND, QUICKSAND, GRAVEL, GLACIAL DRIFT, Boulders, CONGLOMERATE, ROCK, GALS AND OTHER MATERIAL TO BE ENCOUNTERED AND WORK TO BE PERFORMED.

DRAWN BY *L.D.T.T.C.*
CHECKED BY *C.M.C.*
EXAMINED BY *L.P. Gray*

THE METROPOLITAN SANITARY DISTRICT
OF GREATER CHICAGO
CALUMET SEWAGE TREATMENT WORKS
DIVISION X_D

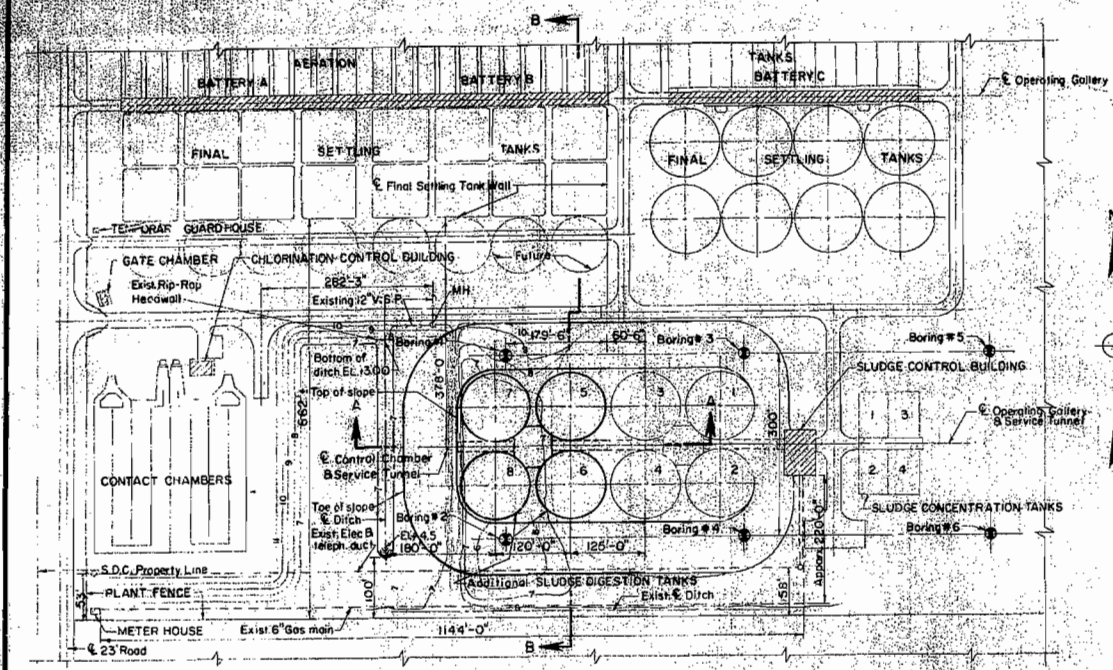
BORINGS
SCALE: *1" = 5'*
SEPTEMBER, 1963
SHEET NO. P-3
1206/1150



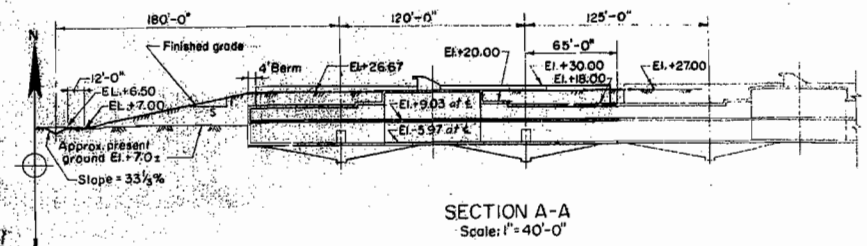
LEGEND:
 — Work under Division Xd
 — Existing structures, roads etc.

Approved: *Raymond J. Winkler*
 Engr. of Treat. Plant Division
 Approved: *Fernand C. Mendez*
 Assistant Civil Engineer
 Approved to: *Philip J. Wilson*
 Chief of M. & S.
 Approved: *E. T. Minkler*
 Civil Engineer

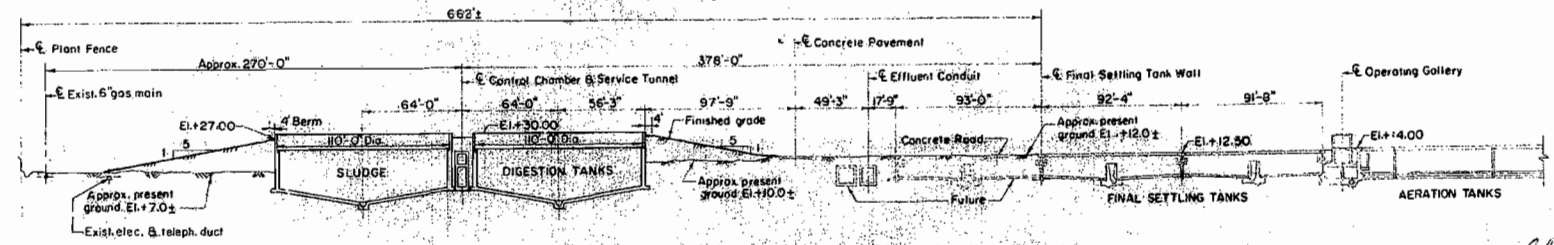
THE METROPOLITAN SANITARY DISTRICT
 OF GREATER CHICAGO
 CALUMET SEWAGE TREATMENT WORKS
 DIVISION Xd
**ADDITIONAL SLUDGE DIGESTION TANKS
 LOCATION PLAN**
 67 203 2 P AUGUST, 1967
 SCALE: 1"=200'-0"
 200 100 0 200
 SHEET NO. P-1



PLAN
Scale: 1"=100'-0"



SECTION A-A
Scale: 1"=40'-0"



SECTION B-B
Scale: 1"=40'-0"

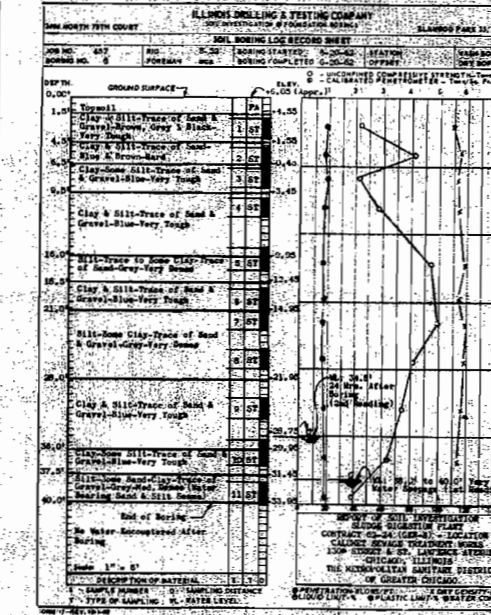
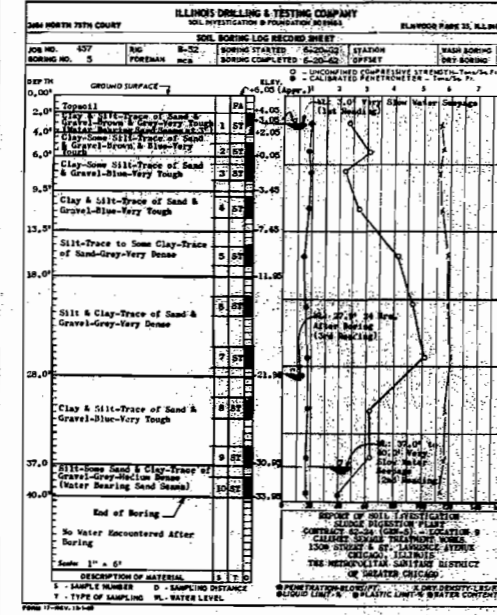
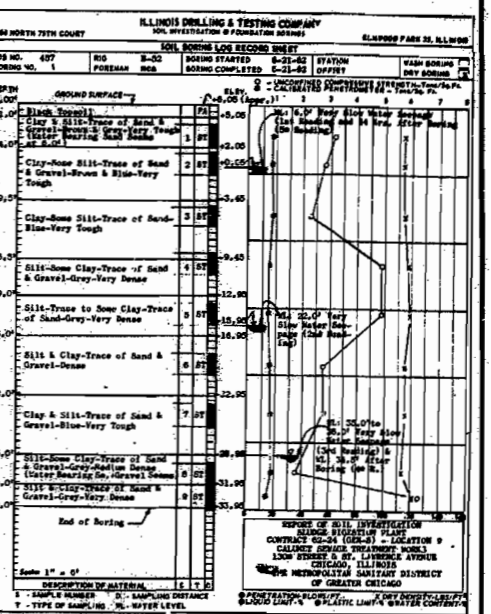
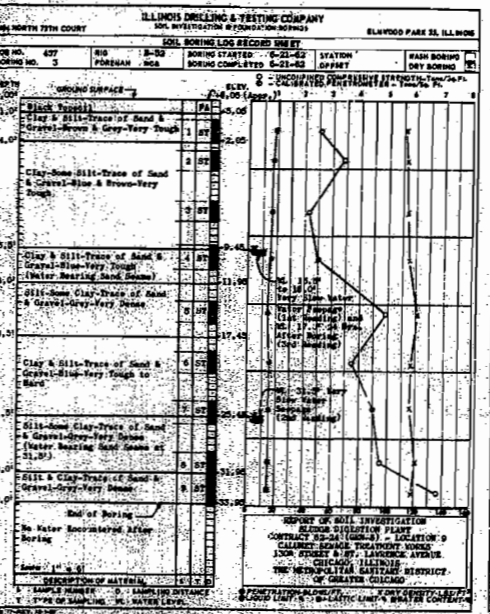
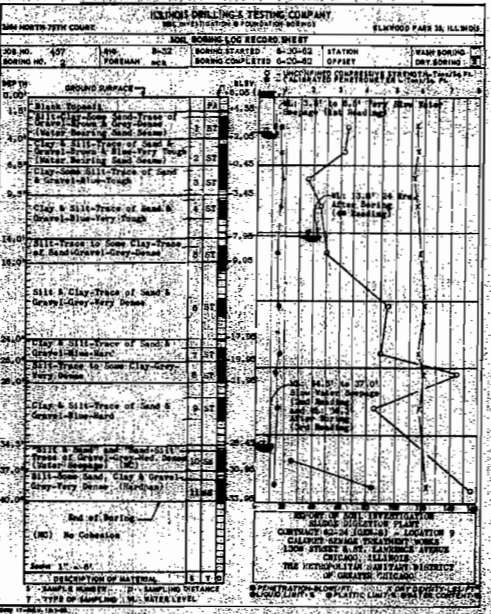
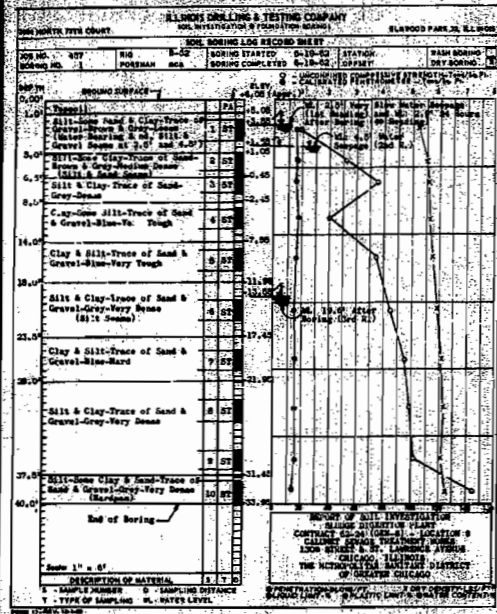
LEGEND
 - - - - - Work under Division Xd
 --- Existing structures and roads

NOTE
 1. The contractor shall verify all dimensions, elevations and locations of existing structures and piping by field measurements.

DRAWN BY: C.R.
 CHECKED BY: [Signature]
 EXAMINED BY: [Signature]

Approved: [Signature]
 Insp. of Trans. Plant Design
 Approved: [Signature]
 Assistant Chief Engineer
 Approved: [Signature]
 Chief of M. & O.
 Approved: [Signature]
 Chief Engineer

Charles J. Simon
 AS BUILT
 THE METROPOLITAN SANITARY DISTRICT
 OF GREATER CHICAGO
 CALUMET SEWAGE TREATMENT WORKS
 DIVISION Xd
 67 203 2 P
 TOPOGRAPHY AND GRADING
 SCALE: AS SHOWN
 AUGUST, 1967
 SHEET NO. P-2



NOTING LOGS
 WHILE THIS INFORMATION IS BELIEVED TO BE ACCURATE, THE
 SANITARY DISTRICT DOES NOT GUARANTEE THE SAME. THE CON-
 TRACTOR MUST TAKE CARE HIMSELF BY MAKING BORINGS OR TEST
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 THE CHARACTER, LOCATION AND DEPTHS OF WATER, PEAT, CLAY,
 SAND, QUICKSAND, GRAVEL, GLACIAL DEPOSIT, Boulders, CON-
 GLOMERATE, ROCK, GAS AND OTHER MATERIAL TO BE ENCOUNTERED
 AND WORK TO BE PERFORMED.

DRAWN BY L.D.T. & C.
 CHECKED BY E.S.L.C.
 EXAMINED BY R.P.M. Gentry

Corrected Raymond Wood
 Engineer of Plant Design
 Approved James J. ...
 Assistant Chief Engineer
 Approved As Philip J. ...
 To Operations Chief of M. & O.
 Approved E.T. ...
 Chief Engineer

Charles Pearson
AS BUILT
 CORRECT
 E. J. ALBRECHT CO. TECH. ENGR.
 THE METROPOLITAN SANITARY DISTRICT
 OF GREATER CHICAGO
 CALUMET SEWAGE TREATMENT WORKS
 DIVISION Xd
 67-208 & P
 TEST PITS AND BORINGS
 AUGUST, 1967
 SHEET NO. P-3

AF 7/74

APPENDIX F

COST ESTIMATE BREAKDOWN TABLES

Electronic Filing - Received, Clerk's Office, October 20, 2008

NSWRP CAPITAL COST ESTIMATION FOR ULTRAVIOLET DISINFECTION SYSTEM AND LOW LIFT PUMP STATION

A. GENERAL SITEWORK

DIVISION	ITEM DESCRIPTION	UNITS	NO.	MATERIAL & LABOR UNIT COST	INSTALLED COST TOTAL	REMARKS
1	GENERAL REQUIREMENTS (Field personnel, Field Offices, Testing & Misc. Project Overheads)				\$1,682,710	15% of Installed Cost for all divisions
2	SITWORK					
	General Equipment Mobilization/Demob (not including pile driving equipment)	LS	1	\$10,000.00	\$10,000	
	Road work (Concrete Pavement)	SY	3,710	\$232.81	\$863,735	
	Site Excavation (not structures or conduits)	CY	3,056	\$2.68	\$8,194	Embankment excavation by BH and onsite stock
	Fencing Removal	LF	1,625	\$6.44	\$10,472	posts every 20'
	Fencing	LF	1,524	\$49.69	\$75,729	
	Fence Gates (20')	Ea	2	\$3,574	\$7,147	
	Clearing and Grubbing	SF	238,737	\$0.50	\$119,369	converted unit to SF
	Strip topsoil and stockpile	SY	13,889	\$1.43	\$19,854	
	Final Grading	SY	13,889	\$1.00	\$13,889	
	Sheeting/Shoring	SF	8,340	\$43.99	\$366,882	+50% for weekend work only
	Retaining Wall (15'H)	LF	530	\$2,105.00	\$1,115,650	Adjusted to remove sub profit
	Hand Mining/Connection/Bulkheading at U/S Connection	LS	1	\$450,000.00	\$450,000	
	Bulkheading and Removal at Gate Structure #3	LS	1	\$120,000.00	\$120,000	
	Misc. Utility Demolition	LF	1,300	\$12.31	\$16,009	
	Erosion Control/Final Seeding	SF	250,000	\$0.40	\$99,918	
	Silt Fence	LF	2,500	\$3.00	\$7,500	
	Survey, Construction Staking	Days	120	\$1,095.52	\$131,462	
	Temporary Power Feed	Ea	2	\$5,000.00	\$10,000	
	Temporary Connections	Ea	10	\$500.00	\$5,000	
	Temporary Heating	SF	14,100	\$11.86	\$167,189	
	Temporary Lighting	SF	14,100	\$14.40	\$203,039	
	Power Use for Temporary Facilities	cst/Mo	131	\$3.14	\$4,936	
	Water Bill	Mo	36	\$70.30	\$2,531	
	Temp Access Road	SY	1,225	\$10.83	\$13,262	Assume 33% of final roadway
	CPM Scheduling	Proj	65.4 mil	0.04%	\$26,160	
	Cleaning	Proj	65.4 mil	0.30%	\$196,200	
	Commissioning	Proj	65.4 mil	0.50%	\$327,000	
	Special Equipment Startup	Days	50	\$725.82	\$36,291	UV Equipment - 25 days, Pumps 25 days
	PIPES					
	Steam (12" dia) & Condensate Return (4" dia)	LF	475	\$420.00	\$199,500	
	Drain (24" dia)	LF	550	\$379.85	\$208,918	
	Non-potable Water (6" dia)	LF	490	\$55.70	\$27,293	
	WNP Hydrants	Ea	4	\$1,874.69	\$7,499	
	Storm Sewer (24" RCP)	LF	660	\$128.38	\$84,731	
	City Water (6" dia)	LF	145	\$55.70	\$8,077	
	Potable Fire Hydrants	Ea	4	\$1,874.69	\$7,499	
	3" STL Casing Pipe with 1" PVC Sampling Line	LF	45	\$47.62	\$2,143	
	Effluent (36" RCP)	LF	500	\$207.12	\$103,560	
	EFFLUENT CONDUITS					
	Conduit, Effluent to Gate Structure (GS) # 1	LF	25	\$2,869.00	\$71,725	
	Conduit, GS1 to GS2	LF	425	\$2,161.00	\$918,425	
	Conduit, GS1 to LLPS	LF	52	\$2,869.00	\$149,188	
	Conduit, LLPS to UV Bldg	LF	100	\$2,869.00	\$286,900	
	Conduit, UV Bldg to GS2	LF	120	\$2,869.00	\$344,280	
	Conduit, GS2 to GS3	LF	115	\$3,191.00	\$366,965	
	MANHOLES					
	Manholes	Ea	19	\$2,542.54	\$48,308	Excavation/Backfill Incidental to Pipe
	Drop Manholes	Ea	1	\$9,249.82	\$9,250	+25% for drop manhole
	Inlet/Catch Basin	Ea	24	\$1,318.14	\$31,635	Excavation/Backfill Incidental to Pipe
	GATE STRUCTURES					
	GS1					
	Excavation	CY	583	\$24.07	\$14,031	
	General Backfill	CY	96	\$7.09	\$681	
	Engineered Backfill	CY	65	\$25.13	\$1,634	
	Disposal of Spoil	CY	487	\$19.65	\$9,569	
	Piling Mobilization	CY	1	\$13,942.98	\$13,943	
	Concrete Filled Pipe Piles (50')	LF	1,500	\$67.37	\$101,057	Adjusted for VLF
	Pile Load Test	Ea	1	\$18,805.44	\$18,805	
	Temporary Sheeting/Shoring	SF	2,160	\$29.39	\$63,473	
	Dewatering	LS	1	\$5,000.00	\$5,000	
	Concrete					
	Base Slabs (includes labor)	CY	41	\$500.00	\$20,500	
	Walls (includes labor)	CY	88	\$920.00	\$80,960	
	Elevated Slabs (includes labor)	CY	41	\$1,000.00	\$41,000	
	Gates	Ea	2	\$90,000.00	\$180,000	Material Only
	Gate installation	Ea	2	\$27,000.00	\$54,000	Installation
	Hatch (SS)	Ea	1	\$10,170.00	\$10,170	
	GS2					
	Excavation	CY	867	\$24.07	\$20,865	
	General Backfill	CY	263	\$7.09	\$1,864	
	Engineered Backfill	CY	59	\$25.13	\$1,483	
	Disposal of Spoil	CY	604	\$19.65	\$11,868	
	Piling Mobilization	LS	1	\$13,942.98	\$13,943	
	Concrete Filled Pipe Piles (50')	LF	1,500	\$67.37	\$101,057	Adjusted for VLF
	Pile Load Test	Ea	1	\$18,805.44	\$18,805	
	Temporary Sheeting/Shoring	SF	3,038	\$29.39	\$89,274	
	Dewatering	LS	1	\$5,000.00	\$5,000	
	Concrete					
	Base Slabs (includes labor)	CY	36	\$500.00	\$18,000	
	Walls (includes labor)	CY	147	\$920.00	\$135,240	
	Elevated Slabs (includes labor)	CY	36	\$1,000.00	\$36,000	
	Gates	Ea	2	\$90,000.00	\$180,000	Material Only
	Gate installation	Ea	2	\$27,000.00	\$54,000	Installation
	Hatch (SS)	Ea	2	\$10,170.00	\$20,340	

Electronic Filing - Received, Clerk's Office, October 20, 2008

NSWRP CAPITAL COST ESTIMATION FOR ULTRAVIOLET DISINFECTION SYSTEM AND LOW LIFT PUMP STATION

GS3					
	Excavation	CY	2,008	\$24.07	\$48,325
	General Backfill	CY	521	\$7.09	\$3,693
	Engineered Backfill	CY	122	\$25.13	\$3,066
	Disposal of Spoil	CY	1,487	\$19.65	\$29,218
	Dewatering	LS	1	\$25,000.00	\$25,000
	Concrete				
	Base Slabs (includes labor)	CY	285	\$500.00	\$142,500
	Walls (includes labor)	CY	46	\$920.00	\$42,320
	Elevated Slabs (includes labor)	CY	13	\$1,000.00	\$13,000
	Bulkhead Installation & Removal	LS	1	\$150,000.00	\$150,000
	Gates	Ea	1	\$90,000.00	\$90,000
	Gate installation	Ea	2	\$27,000.00	\$54,000
	Hatch (SS)	Ea	1	\$10,170.00	\$10,170
					Material Only
					Installation
16	ELECTRICAL DUCT BANK				
	6 cells, 5" conduit from Battery E to UV Building	LF	1,020	\$200.00	\$204,000
	6 cells, 5" conduit from UV Building to PS	LF	140	\$200.00	\$28,000
	4 cells, 5" conduit from UV Building to Pump and Blower Bldg.	LF	1,000	\$160.00	\$160,000
	500 kcmil (15 kV)	LF	4,710	\$20.00	\$94,200
	4/0 AWG (600 V)	LF	690	\$7.00	\$4,830
	Fiber Optic Cable	LF	1,850	\$95.00	\$175,750
	Electrical Manholes	Ea	18	\$12,500.00	\$225,000
	TRANSFORMER YARD (*70% OF COST ALLOCATED TO UV)				
	Switchgear Yard, 50ft x 50ft, fence and stone	LS	1	\$50,000.00	\$35,000*
	Medium-Voltage Air Interrupter Switchgear				
	Transformer Primary Switch, 38KV, 600A	EA	2	\$99,000.00	\$138,600*
	Motor operated main and tie switches, 15 KV, 600A	EA	3	\$54,800.00	\$115,080*
	Feeder switches, 15 KV, 600A	EA	4	\$54,800.00	\$153,440*
	Substation Transformers	MVA	20	\$99,100.00	\$547,400*
	Site Lighting Poles	Ea	10	\$3,280.70	\$32,807
	Battery E Switchgear Modifications	LS	1	\$66,792.00	\$66,792
					Cost is allocated proportionally between Battery E, Tertiary Filters, and UV.
					UV is 70% of total (5 MVA of 7MVA)
					Labor = 20% of material cost
	SUBTOTAL				\$12,900,777
	GC Markup on Subs @ 5% (except for General Conditions)				\$560,903
	Subtotal				\$13,461,680
	Escalation to Midpoint of Construction @ 7.5%				\$1,009,626
	Subtotal				\$14,471,306
	Contractor OH&P @ 15%				\$2,019,252
	Subtotal				\$15,480,932
	Planning Level Contingency @ 30%				\$4,644,280
	Subtotal				\$20,125,212
	Misc. Capital Costs				
	Legal and Fiscal Fees @ 15%				\$3,018,782
	Engineering Fees including CM @ 20%				\$4,025,042
	Subtotal				\$7,043,824
	GENERAL SITEWORK PROJECT TOTAL				\$27,170,000

Electronic Filing - Received, Clerk's Office, October 20, 2008

NSWRP CAPITAL COST ESTIMATION FOR ULTRAVIOLET DISINFECTION SYSTEM AND LOW LIFT PUMP STATION

B. LOW LIFT PUMP STATION

DIVISION	ITEM DESCRIPTION	UNITS	NO.	MATERIAL UNIT COST	INSTALLED COST TOTAL	REMARKS
1	GENERAL REQUIREMENTS (Field personnel, Field Offices, Testing & Misc. Project Overheads)				\$1,618,783	15% of Installed Cost for all divisions
2	SITWORK					
	Excavation	CY	12,500	\$24.07	\$300,828	
	General Backfill	CY	609	\$7.09	\$4,317	
	Engineered Backfill	CY	260	\$25.13	\$6,534	
	Disposal of Spoil	CY	11,891	\$19.65	\$233,647	
	Piling Mobilization	LS	1	\$13,942.98	\$13,943	
	Concrete Filled Pipe Piles (50')	LF	10,000	\$67.37	\$673,715	
	Pile Load Test	Ea	3	\$18,805.44	\$56,416	
	Temporary Sheeting/Shoring	SF	10,530	\$29.39	\$309,431	
	Dewatering	LS	1	\$40,000	\$40,000	
3	CONCRETE					
	Base Slabs (includes labor)	CY	885	\$500.00	\$442,500	
	Walls (includes labor)	CY	391	\$920.00	\$359,720	
	Elevated Slabs (includes labor)	CY	124	\$1,000.00	\$124,000	
4	MASONRY					
	Exterior Walls	SF	13,850	\$45.00	\$623,250	Revised up due to complex features
5	METALS					
	Handrails and Railings	LF	900	\$100.00	\$90,000	
	Structural Steel	TONS	53	\$5,000	\$265,000	
	SS Ladder (Roof Access)	LF	40	\$745.80	\$29,832	
	Metal Stairs	Ea	3	\$8,000.00	\$24,000	
	Metal Decking (Roof) (includes insulation)	SF	4,600	\$3.10	\$14,243	
6	WOOD & PLASTICS				\$0	
7	THERMAL & MOISTURE PROTECTION					
	Roofing System	SF	4,600	\$7.00	\$32,200	
	Roof Drainage System	SF	4,600	\$1.00	\$4,600	
8	DOORS & WINDOWS					
	Doors (SS)	Ea	6	\$6,500	\$39,000	
	Windows	SF	1,310	\$25	\$32,750	
	Skylights	SF	567	\$45	\$25,515	
	Overhead Door	Ea	1	\$15,000	\$15,000	
	Submerged Manways	Ea	4	\$7,500	\$30,000	
	Hatches (SS)	Ea	3	\$10,170	\$30,510	
9	FINISHES					
	High Performance Coating (Walls)	SF	11,480	\$2.00	\$22,960	
	Floor Coating	SF	4,600	\$2.25	\$10,350	
10	SPECIALITIES				\$0	
11	EQUIPMENT					
	Pumps (includes motors)	Ea	6	\$729,250	\$4,375,500	Installation = 25% Eqpm. Cost
	Perforated Plate Baffles	Ea	6	\$36,500	\$219,000	
13	SPECIAL CONSTRUCTION (incl. INSTRUMENTATION)					
	Lightning Protection Systems	LS	1	\$7,080	\$7,080	
	Distributed Control System (DCS) Modifications	LS	1	\$40,000	\$40,000	
	Input/Output (I/O) Point List	EA	109	\$1,500	\$163,500	
14	CONVEYING SYSTEMS					
	Bridge Crane/Hoist	LS	1	\$85,466	\$85,466	Installation = 40% Eqpm. Cost
15	MECHANICAL					
	Plant Water	LS	1	\$20,000	\$20,000	
	City Water	LS	1	\$20,000	\$20,000	
	Slide Gates	Ea	4	\$117,000	\$468,000	+30% for installation
	Slide Gates (Bonnet)	Ea	2	\$234,000	\$468,000	+30% for installation
	Plug Valves (8")	Ea	2	\$1,300	\$2,600	
	Motorized Louvres, Med	Ea	4	\$2,000	\$8,000	
	Exhaust Fans, Wall	Ea	6	\$2,800	\$16,800	
	Unit Heaters, Suspended	Ea	6	\$2,000	\$12,000	
	Building Plumbing	LS	1	\$25,000	\$25,000	
	Butterfly Valves (60")	Ea	6	\$30,000	\$180,000	+20% For Installation
	Flap Gate (60")	Ea	6	\$12,000	\$72,000	+20% For Installation
16	ELECTRICAL					
	Building Systems					
	Basic Material	SF	4,600	\$4.62	\$21,260	
	Devices	SF	4,600	\$0.35	\$1,611	
	Equipment Connections	SF	4,600	\$2.67	\$12,267	
	Service & Distribution	SF	4,600	\$2.11	\$9,720	
	Lighting	SF	4,600	\$5.65	\$25,990	
	Intercom System	SF	4,600	\$0.47	\$2,183	
	Fire Alarm & Detection	SF	4,600	\$0.51	\$2,339	
	Low Voltage Switchgear					
	Main Breaker, 3000A w/ Metering	EA	2	\$77,114	\$154,228	
	Tie Breaker, 3000A	EA	1	\$74,614	\$74,614	
	Feeder Breaker, 1600A	EA	6	\$36,348	\$218,088	
	Space for Future Breaker	EA	2	\$5,500	\$11,000	
	MCC RVSS	Ea	4	\$22,500	\$90,000	
	Variable Frequency Drive, 250 horsepower	EA	2	\$65,688	\$131,375	
	SUBTOTAL				\$12,410,667	
	GC Markup on Subs @ 5% (except for General Conditions)				\$539,594	
	Subtotal				\$12,950,261	A
	Escalation to Midpoint of Construction @ 7.5%				\$971,270	B = A X 0.075
	Subtotal				\$13,381,936	A+B
	Contractor OH&P @ 15%				\$2,007,290	C = (A+B) X 0.15
	Subtotal				\$15,389,227	A+B+C
	Planning Level Contingency @ 30%				\$4,616,768	D = (A+B+C) x 0.3
	Subtotal				\$20,005,995	A+B+C+D
	Misc. Capital Costs					
	Legal and Fiscal Fees @ 15%			\$3,000,899		E = (A+B+C+D) x 0.15
	Engineering Fees including CM @ 20%			\$4,001,199		F = (A+B+C+D) x 0.2
	Subtotal			\$7,002,098		E+F
	LOW LIFT PUMP STATION PROJECT TOTAL				\$27,010,000	A+B+C+D+E+F

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NSWRP CAPITAL COST ESTIMATION FOR ULTRAVIOLET DISINFECTION SYSTEM AND LOW LIFT PUMP STATION

C. UV DISINFECTION BUILDING

DIVISION	ITEM DESCRIPTION	UNITS	NO.	MATERIAL UNIT COST	INSTALLED COST TOTAL	REMARKS
1	GENERAL REQUIREMENTS (Field personnel, Field Offices, Testing & Misc. Project Overheads)				\$2,965,715	15% of Installed Cost for all divisions
2	SITWORK					
	Excavation	CY	6,000	\$24.07	\$144,398	
	General Backfill	CY	2,300	\$7.09	\$16,304	
	Engineered Backfill	CY	400	\$25.13	\$10,053	
	Disposal of Spoil	CY	3,700	\$19.65	\$72,701	
	Piling Mobilization	LS	1	\$13,942.98	\$13,943	
	Concrete Filled Pipe Piles (50')	LF	16,000	\$67.37	\$1,077,944	
	Pile Load Test	Ea	3	\$18,805.44	\$56,416	
	Temporary Sheeting/Shoring	SF	8,000	\$29.39	\$235,086	
	Dewatering	LS	1	\$25,000.00	\$25,000	
3	CONCRETE					
	Base Slabs (includes labor)	CY	900	\$500.00	\$450,000	
	Walls (includes labor)	CY	930	\$920.00	\$855,600	
	Elevated Slabs (includes labor)	CY	500	\$1,000.00	\$500,000	
4	MASONRY					
	Interior Walls	SF	2,067	\$25.00	\$51,675	
	Exterior Walls	SF	6,500	\$45.00	\$292,500	Revised up due to complex features
5	METALS					
	SS Ladder (Roof Access)	LF	16	\$745.80	\$11,933	
	Structural Steel	Tons	1	\$5,000.00	\$5,000	
	Gratings	SF	1,300	\$30.00	\$39,000	
6	WOOD & PLASTICS					
	Misc Blocking	LS	1	\$5,000.00	\$5,000	
7	THERMAL & MOISTURE PROTECTION					
	Roofing System	SF	8,550	\$7.00	\$59,850	
	Roof Drainage System	SF	8,550	\$1.00	\$8,550	
8	DOORS & WINDOWS					
	Doors (SS)	Ea	11	\$6,500	\$71,500	
	Windows	SF	1,030	\$25.00	\$25,750	
	Skylights	SF	480	\$30.00	\$14,400	
	Overhead Door	Ea	1	\$15,000.00	\$15,000	
	Hatches	Ea	3	\$10,170.00	\$30,510	
9	FINISHES					
	High Performance Coatings (walls)	SF	8,000	\$2.00	\$16,000	
	Floor Coating	SF	5,007	\$2.25	\$11,266	
	Acoustic Ceiling	SF	2,000	\$4.00	\$8,000	
10	SPECIALITIES				\$0	
11	EQUIPMENT					
	UV Reactors	LS	1	\$10,339,140.55	\$10,339,141	Installation = 15% Eqpm. Cost
	Effluent Sampling System, Pump/Sampler	LS	1	\$10,000.00	\$10,000	
13	SPECIAL CONSTRUCTION (incl. INSTRUMENTATION)					
	Lighting Protection Systems	LS	1	\$7,080.00	\$7,080	
	Distributed Control System (DCS) Modifications	LS	1	\$40,000.00	\$40,000	
	Input/Output (I/O) Point List	EA	164	\$1,000.00	\$164,000	
14	CONVEYING SYSTEMS				\$0	
15	MECHANICAL					
	Misc. Piping	LS	1	\$25,000.00	\$25,000	
	Weir Gates, Motorized	Ea	5	\$169,000.00	\$845,000	+30% for installation
	Slide Gates, Motorized	Ea	5	\$188,500.00	\$942,500	+30% for installation
	Motorized Louvres, Med	Ea	2	\$860.00	\$1,720	
	Motorized Louvres, Large	Ea	2	\$2,000.00	\$4,000	
	Exhaust Fans, Wall	Ea	3	\$1,300.00	\$3,900	
	Exhaust Fans, Roof	Ea	3	\$3,125.00	\$9,375	
	Unit Heaters, Suspended	Ea	5	\$2,000.00	\$10,000	
	Unit Heaters, Overhead	Ea	2	\$4,500.00	\$9,000	
	Air Handling Units	Ea	1	\$3,500.00	\$3,500	
	AHU/ACCU	Ea	1	\$10,500.00	\$10,500	
	Building Plumbing	LS	1	\$10,000.00	\$10,000	
	Flow Meters, A/V	Ea	2	\$20,190.00	\$40,380	+20% for installation
	Mud Valves	Ea	5	\$1,000.00	\$5,000	
	Hatches, Special	Ea	10	\$15,000.00	\$150,000	
16	ELECTRICAL					
	Building Systems					
	Basic Material	SF	8,550	\$4.62	\$39,516	
	Devices	SF	8,550	\$0.35	\$2,995	
	Equipment Connections	SF	8,550	\$2.67	\$22,801	
	Service & Distribution	SF	8,550	\$2.11	\$18,067	
	Lighting	SF	8,550	\$5.65	\$48,308	
	Intercom System	SF	8,550	\$0.47	\$4,058	
	Fire Alarm & Detection	SF	8,550	\$0.51	\$4,348	
	Medium-Voltage Circuit Breaker Switchgear					
	Main Breaker	EA	2	\$109,050.00	\$218,100	
	Tie Breaker	EA	1	\$109,050.00	\$109,050	
	Feeders (2 high)	EA	7	\$188,364.00	\$1,318,548	
	Feeders (2 high) - Prepared Space	EA	3	\$34,070.00	\$102,210	
	Control Power Section	EA	2	\$48,630.00	\$97,260	
	Control Power Transformer, 75 KVA	EA	2	\$25,250.00	\$50,500	
	Secondary Unit Substations					
	Transformer, 1500 KVA, 80 deg C, VPI	EA	5	\$74,745.00	\$373,725	
	Feeder Breaker, 1600A	EA	12	\$36,348.00	\$436,176	
	Space for Future Breaker	EA	8	\$5,500.00	\$44,000	
	Padmount Transformer, 1500 KVA, Pump Station Service	EA	2	\$64,150.00	\$128,300	
	SUBTOTAL				\$22,737,150	
	GC Markup on Subs @ 5% (except for General Conditions)				\$988,572	
	Subtotal				\$23,725,722	A
	Escalation to Midpoint of Construction @ 7.5% (18 months to midpoint)				\$1,779,429	B = A X 0.075
	Subtotal				\$24,516,579	A+B
	Contractor OH&P @ 15%				\$3,677,487	C = (A+B) X 0.15
	Subtotal				\$28,194,066	A+B+C
	Planning Level Contingency @ 30%				\$8,458,220	D = (A+B+C) x 0.3
	Subtotal				\$36,652,286	A+B+C+D
	Misc. Capital Costs					
	Legal and Fiscal Fees @ 15%				\$5,497,843	E = (A+B+C+D) x 0.15
	Engineering Fees including CM @ 20%				\$7,330,457	F = (A+B+C+D) x 0.2
	Subtotal				\$12,828,300	E+F
	UV DISINFECTION BUILDING PROJECT TOTAL				\$49,490,000	A+B+C+D+E+F
	PROJECT GRAND TOTAL				\$103,670,000	

Electronic Filing - Received, Clerk's Office, October 20, 2008

NSWRP ANNUAL O&M COSTS FOR UV DISINFECTION SYSTEM AND LOW LIFT PUMP STATION

PRESENT WORTH FACTOR	
Life, N	20
Ineterest, i	4.875
Inflation, j	3
Present Worth Factor	23.17

Average Energy Cost, \$/kWh	\$0.0684
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A. GENERAL SITEWORK							
Item	Operating (kW)	Time of Operation (hrs/day)	Power Usage (kW-hr/day)	Energy Cost (\$/day)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
OPERATIONS							
Energy - Electrical	10	24	240.0	\$16.42	\$5,994	23.17	\$138,887
Subtotal					\$5,994		\$138,887
	No. of Operators (per day)	Time (hrs/day/operator)	Total Time (hrs/day)	Labor Rate (\$/hr)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
MAINTENANCE							
Routine Maintenance	1	2	2	\$95.00	\$69,350	23.17	\$1,606,840
Labor - Operator	0	0	0	\$95.00	\$0	23.17	\$0
Electrician	0	0	0	\$165.00	\$0	23.17	\$0
Subtotal					\$69,350		\$1,606,840
	Construction Cost of New Equip. & Piping (\$)	% for Annual Parts & Supplies			Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
PARTS AND SUPPLIES							
Parts and Supplies	1,099,218	5%			\$54,961	23.17	\$1,273,444
Subtotal					\$54,961		\$1,273,444
General Sitework Total Annual O&M					\$130,305		
General Sitework Total Present Worth O&M Cost							\$3,019,171

B. LOW LIFT PUMP STATION							
Item	Operating (kW)	Time of Operation (hrs/day)	Power Usage (kW-hr/day)	Energy Cost (\$/day)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
OPERATIONS							
Energy - Electrical (333 MGD Avg Q)	375	24	9000.0	\$615.85	\$160,121	23.17	\$3,709,994
Subtotal					\$160,121		\$3,709,994
	No. of Operators (per day)	Time (hrs/day/operator)	Total Time (hrs/day)	Labor Rate (\$/hr)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
MAINTENANCE							
Routine Maintenance	2	2	4	\$95.00	\$138,700	23.17	\$3,213,679
Labor - Operator	2	8	16	\$95.00	\$395,200	23.17	\$9,156,784
Electrician	1	1	1	\$165.00	\$60,225	23.17	\$1,395,413
Subtotal					\$594,125		\$13,765,876
	Construction Cost of New Equip. & Piping (\$)	% for Annual Parts & Supplies			Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
PARTS AND SUPPLIES							
Parts and Supplies	6,998,132	5%			\$349,907	23.17	\$8,107,336
Subtotal					\$349,907		\$8,107,336
Low Lift Pump Station Total Annual O&M					\$1,104,152		
Low Lift Pump Station Total Present Worth O&M Cost							\$25,583,206

C. DISINFECTION SYSTEM							
Item	Operating (kW)	Time of Operation (hrs/day)	Power Usage (kW-hr/day)	Energy Cost (\$/day)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
OPERATIONS							
Energy - Electrical	3,182	24	76,368	\$5,225.68	\$1,358,677	23.17	\$31,480,540
Subtotal					\$1,358,677		\$31,480,540
*Annual Energy Costs based on 24 hours operation for 9 months (March thru November)							
	No. of Operators (per day)	Time (hrs/unit-time/operator)	Total Time (hrs/unit-time)	Labor Rate (\$/hr)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
MAINTENANCE							
Electrician for routine maintenance	1	2 per week	2 per week	\$165.00	\$12,257	23.17	\$283,998
Electrician to replace UV lamps	2	8 per week	16 per week	\$165.00	\$137,657	23.17	\$3,189,516
Electrician for lamp cleaning/inspection	2	40 per week	80 per week	\$165.00	\$688,286	23.17	\$15,947,580
Labor - Operator	2	8 per day	16 per day	\$95.00	\$395,200	23.17	\$9,156,784
Subtotal					\$1,233,400		\$28,577,878
*Annual Maintenance Costs based on - (a) operation for 9 months (March thru November); (b) based on 365 days only for lamp replacement.							
	Construction Cost of New Equip. & Piping (\$)	% for Annual Parts & Supplies	Number of Units Replaced per Year	Cost per Unit (\$)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
PARTS AND SUPPLIES							
Parts and Supplies	5,308,916	5%			\$265,446	23.17	\$6,150,379
Lamp (replacement)			1680	\$215.00	\$361,200	23.17	\$8,369,004
Ballast (replacement)			336	\$877.50	\$294,840	23.17	\$6,831,443
Quartz sleeve (replacement)			168	\$338.00	\$56,784	23.17	\$1,315,685
Scraper wiper (replacement)			560	\$40.00	\$22,400	23.17	\$519,008
Subtotal					\$1,000,670		\$23,185,519
UV System Total Annual O&M					\$3,592,747		
UV System Total Present Worth O&M Cost							\$83,243,937
Project Grand Total Annual O&M					\$4,830,000		
Project Total Present Worth O&M Cost							\$111,900,000

Electronic Filing - Received, Clerk's Office, October 20, 2008

A. NSWRP UV PILOT PLANT

DIVISION	ITEM DESCRIPTION	UNITS	NO.	UNIT COST	INSTALLED COST
					TOTAL
1	General Requirements	LS	1		\$149,630
2	Site Work	SF	10,000	\$15	\$150,000
3	Concrete Channel	LF	100	\$1,450	\$145,000
3	Gates	Ea	2	\$75,000	\$150,000
3	Discharge Piping (48" RCP)	LF	500	\$12	\$6,064
3	Trenching and Backfill	LF	500	\$11	\$5,320
11	UV Reactor (20 MGD)	Ea	1	\$350,000	\$350,000
10	Metal Sandwich Building	SF	1200	\$134	\$161,150
16	Temporary Power	LS	1	\$30,000	\$30,000
	SUBTOTAL				\$997,534
	GC Markup on Subs @ 5% (except for General Condi				\$49,877
	Subtotal				\$1,047,411
	Escalation to Midpoint of Construction @ 7.5% (18 m				\$78,556
	Subtotal				\$1,076,090
	Contractor OH&P @ 15%				\$161,413
	Subtotal				\$1,237,503
	Planning Level Contingency @ 30%				\$371,251
	Subtotal				\$1,608,754
	Misc. Capital Costs				
	Legal and Fiscal Fees @ 15%				\$241,313
	Engineering Fees including CM @ 20%				\$321,751
	Subtotal				\$563,064
	NSWRP PILOT PLANT PROJECT TOTAL				\$2,180,000

Electronic Filing - Received, Clerk's Office, October 20, 2008

A. NSWRP ComEd Service					
DIVISION	ITEM DESCRIPTION	UNITS	NO.	UNIT COST	INSTALLED COST TOTAL
1	General Requirements	LS	1		\$176,723
2	Miscellaneous Restoration	SF	10,000	\$15	\$150,000
	Underground Duct (Service from TSS-85)				
	6 cells, 5" conduit from Battery E to UV Building	LF	120	\$200.00	\$24,000
	500 kcmil (15 kV)	LF	540	\$20.00	\$10,800
	Electrical Manholes	Ea	2	\$12,500.00	\$25,000
	ComEd Second Service				
	Flagman (2)	Days	30	\$ 1,050.00	\$ 31,500.00
	Digging holes in earth	EA	50	\$ 436.20	\$ 21,810.13
	Wood electric utility pole, 45ft	EA	50	\$ 1,788.34	\$ 89,416.90
	Wood poles, material handling and spotting	EA	50	\$ 611.91	\$ 30,595.32
	Erect poles& backfill holes in earth	EA	50	\$ 3,113.72	\$ 155,685.75
	Double Crossarm, each 10 ft x 3-1/2 in x 4-1/2 in	EA	50	\$ 1,115.17	\$ 55,758.72
	Double Crossarm, each 8 ft x 3-1/2 in x 4-1/2 in	EA	50	\$ 1,036.21	\$ 51,810.50
	Crossarm, material handling and spotting	EA	50	\$ 273.04	\$ 13,652.10
	Install crossarm	EA	50	\$ 1,490.13	\$ 74,506.55
	Conductor, 795 to 954	W-Mi	6	\$ 21,119.70	\$ 126,718.20
	Wire, material handling and spotting	W-Mi	6	\$ 1,116.55	\$ 6,699.32
	Insulators, Pedestal type	EA	300	\$ 125.68	\$ 37,703.58
	Overhead ground wire	W-Mi	2	\$ 10,766.64	\$ 21,533.28
	Overhead ground wire, material handling and spotting	W-Mi	2	\$ 702.40	\$ 1,404.79
	ROW clearing	acre	7	\$ 964.41	\$ 6,750.87
	ROW restoration	acre	7	\$ 1,933.48	\$ 13,534.33
	Surveying	LS	1	\$113,000.00	\$ 113,000.00
	Soil Boring	LS	1	\$ 16,272.00	\$ 16,272.00
16	Substation Modifications				
	TSS-85 Protective Device Adjustment	LS	1	\$ 50,000.00	\$ 50,000.00
	TSS-88 Protective Device Adjustment	LS	1	\$ 50,000.00	\$ 50,000.00
	SUBTOTAL				\$1,354,875
	GC Markup on Subs @ 5% (except for General Conditions)				\$67,744
	Subtotal				\$1,422,619
	Escalation to Midpoint of Construction @ 0%				\$0
	Subtotal				\$1,422,619
	Contractor OH&P @ 15%				\$213,393
	Subtotal				\$1,636,012
	Planning Level Contingency @ 30%				\$490,804
	Subtotal				\$2,126,815
	Misc. Capital Costs				
	Legal and Fiscal Fees @ 15%				\$319,022
	Engineering Fees including CM @ 20%				\$425,363
	Subtotal				\$744,385
	NSWRP COMED SERVICE IMPROVEMENTS PROJECT TOTAL				\$2,880,000

Electronic Filing - Received, Clerk's Office, October 20, 2008

A. CWRP CHLORINE CONTACT CHAMBER DEMOLITION

DIVISION	ITEM DESCRIPTION	UNITS	NO.	UNIT COST	INSTALLED COST
					TOTAL
2	<u>Demolition</u>				
	Exterior Walls (18")	SF	17395	24.30	\$422,767
	Interior Walls	SF	63840	22.71	\$1,450,006
	Disposal at Landfill	CY	3922	12.89	\$50,554
	Structural Backfill	CY	4002	11.50	\$46,008
	Common Backfill	CY	36021	10.70	\$385,373
	SUBTOTAL				\$2,360,000
	Extended Total				\$4,980,000

Electronic Filing - Received, Clerk's Office, October 20, 2008

CWRP ANNUAL O&M COSTS FOR UV DISINFECTION SYSTEM AND LOW LIFT PUMP STATION

PRESENT WORTH FACTOR	
Life, N	20
Ineterest, i	4.875
Inflation, j	3
Present Worth Factor	23.17

Average Energy Cost, \$/kWh	\$0.0684
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A. GENERAL SITEWORK							
Item	Operating (kW)	Time of Operation (hrs/day)	Power Usage (kW-hr/day)	Energy Cost (\$/day)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
OPERATIONS							
Energy - Electrical	10.67	24	256.0	\$17.52	\$6,394	23.17	\$148,146
Subtotal					\$6,394		\$148,146
	No. of Operators (per day)	Time (hrs/day/operator)	Total Time (hrs/day)	Labor Rate (\$/hr)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
MAINTENANCE							
Routine Maintenance	1	2	2	\$90.00	\$65,700	23.17	\$1,522,269
Labor - Operator	0	0	0	\$90.00	\$0	23.17	\$0
Electrician	0	0	0	\$159.50	\$0	23.17	\$0
Subtotal		NSWRP			\$65,700		\$1,522,269
	Construction Cost of New Equip. & Piping (\$)	% for Annual Parts & Supplies			Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
PARTS AND SUPPLIES							
Parts and Supplies	1,172,499	5%			\$58,625	23.17	\$1,358,341
Subtotal					\$58,625		\$1,358,341
General Sitework Total Annual O&M					\$130,719		
General Sitework Total Present Worth O&M Cost							\$3,028,756

B. LOW LIFT PUMP STATION							
Item	Operating (kW)	Time of Operation (hrs/day)	Power Usage (kW-hr/day)	Energy Cost (\$/day)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
OPERATIONS							
Energy - Electrical (305 MGD Avg Q)	331	24	7944.0	\$543.59	\$141,333	23.17	\$3,274,688
Subtotal					\$141,333		\$3,274,688
	No. of Operators (per day)	Time (hrs/day/operator)	Total Time (hrs/day)	Labor Rate (\$/hr)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
MAINTENANCE							
Routine Maintenance	2	2	4	\$90.00	\$131,400	23.17	\$3,044,538
Labor - Operator	1	8	8	\$90.00	\$187,200	23.17	\$4,337,424
Electrician	1	1	1	\$159.50	\$58,218	23.17	\$1,348,899
Subtotal					\$376,818		\$8,730,861
	Construction Cost of New Equip. & Piping (\$)	% for Annual Parts & Supplies			Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
PARTS AND SUPPLIES							
Parts and Supplies	7,464,674	5%			\$373,234	23.17	\$8,647,825
Subtotal					\$373,234		\$8,647,825
Low Lift Pump Station Total Annual O&M					\$891,384		
Low Lift Pump Station Total Present Worth O&M Cost							\$20,653,375

C. DISINFECTION SYSTEM							
Item	Operating (kW)	Time of Operation (hrs/day)	Power Usage (kW-hr/day)	Energy Cost (\$/day)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
OPERATIONS							
Energy - Electrical	2,903	24	69,672	\$4,767.49	\$1,239,547	23.17	\$28,720,304
Subtotal					\$1,239,547		\$28,720,304
*Annual Energy Costs based on 24 hours operation for 9 months (March thru November)							
	No. of Operators (per day)	Time (hrs/unit-time/operator)	Total Time (hrs/unit-time)	Labor Rate (\$/hr)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
MAINTENANCE							
Electrician for routine maintenance	1	2 per week	2 per week	\$165.00	\$12,257	23.17	\$283,998
Electrician to replace UV lamps	2	8 per week	16 per week	\$165.00	\$137,657	23.17	\$3,189,516
Operator for lamp cleaning/inspectio	2	40 per week	80 per week	\$165.00	\$688,286	23.17	\$15,947,580
Labor - Operator	2	8 per day	16 per day	\$95.00	\$395,200	23.17	\$9,156,784
Subtotal					\$1,233,400		\$28,577,878
*Annual Maintenance Costs based on - (a) operation for 9 months (March thru November); (b) based on 365 days only for lamp replacement.							
	Construction Cost of New Equip. & Piping (\$)	% for Annual Parts & Supplies	Number of Units Replaced per Year	Cost per Unit (\$)	Annual Cost (\$)	Present Worth Factor	Present Worth (\$)
PARTS AND SUPPLIES							
Parts and Supplies	5,662,843	5%			\$283,142	23.17	\$6,560,404
Lamp (replacement)			1680	\$215.00	\$361,200	23.17	\$8,369,004
Ballast (replacement)			336	\$877.50	\$294,840	23.17	\$6,831,443
Quartz sleeve (replacement)			168	\$338.00	\$56,784	23.17	\$1,315,685
Scraper wiper (replacement)			560	\$40.00	\$22,400	23.17	\$519,008
Subtotal					\$1,018,366		\$23,595,544
UV System Total Annual O&M					\$3,491,313		
UV System Total Present Worth O&M Cost							\$80,893,726
Project Grand Total Annual O&M					\$4,520,000		
Project Total Present Worth O&M Cost							\$104,600,000

Electronic Filing - Received, Clerk's Office, October 20, 2008

A. CWRP ComEd Service					
DIVISION	ITEM DESCRIPTION	UNITS	NO.	UNIT COST	INSTALLED COST TOTAL
1	General Requirements	LS	1		\$7,500
16	Substation Modifications				
	TSS-85 Protective Device Adjustment	LS	1	\$ 50,000.00	\$ 50,000.00
	SUBTOTAL				\$57,500
	GC Markup on Subs @ 5% (except for General Conditions)				\$2,875
	Subtotal				\$60,375
	Escalation to Midpoint of Construction @ 0%				\$0
	Subtotal				\$60,375
	Contractor OH&P @ 15%				\$9,056
	Subtotal				\$69,431
	Planning Level Contingency @ 30%				\$20,829
	Subtotal				\$90,261
	Misc. Capital Costs				
	Legal and Fiscal Fees @ 15%				\$13,539
	Engineering Fees including CM @ 20%				\$18,052
	Subtotal				\$31,591
	CWRP COMED SERVICE IMPROVEMENTS PROJECT TOTAL				\$130,000

**DISINFECTION COST STUDY
HYDRAULIC EVALUATION
FOR
METROPOLITAN WATER RECLAMATION
DISTRICT OF GREATER CHICAGO

STICKNEY WATER RECLAMATION PLANT**

TECHNICAL MEMORANDUM

June 2, 2008

Prepared By



303 EAST WACKER DRIVE, SUITE 600
CHICAGO, ILLINOIS 60601

**MWRDGC Project No. 07-026-2P
CTE Project No. 60040695**

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- Appendix B Selected Pages from Chicago Underflow Plan Detailed Design Report (USACE, 1999)
- Appendix C Proposed Layout of Low Lift Pump Station

1 INTRODUCTION

This technical memorandum has been developed as part of the Preliminary Cost Opinion for Ultraviolet (UV) Disinfection Facilities Study at the Metropolitan Water Reclamation District of Greater Chicago's (MWRDGC, or District) Stickney Water Reclamation Plant (SWRP) in Illinois. This memorandum continues the work that began in TM1-WQ which was developed previously as part of a Water Quality (WQ) Strategy for affected Chicago Area Waterways.

The TM1-WQ documented the results of a Consoer Townsend Envirodyne Engineers (CTE) study of effluent disinfection alternatives for the District's North Side, Calumet and Stickney WRPs. Based on economic and non-economic evaluation of alternatives, ozone disinfection and UV disinfection were selected and study-level basis of design and cost estimates were developed. Both alternatives were developed including three components: a low lift pump station, a tertiary filter facility, and a UV or ozone disinfection facility. The need for tertiary filtration to support disinfection was based on limited sampling that showed transmittance values less than the IEPA minimum of 65% and energy savings with a less turbid flow stream. Because of the limited available information, the estimates that were developed were broken into two alternatives for each disinfection technology: one with tertiary filters and one without tertiary filters. In both cases, a low lift pump station was included based on conceptual level evaluations of the available hydraulic driving head for the existing and proposed conditions.

Subsequent to the TM1-WQ evaluation, additional transmittance data was obtained and the District requested that the costs be further developed without including tertiary filtration. This additional evaluation is also based on the comments received from the United States Environmental Protection Agency (USEPA) as part of the Use Attainability Analysis (UAA) evaluations, and new information obtained since the previous work.

1.1 Objective

The primary objectives of the evaluation presented in this technical memorandum are:

- To update the hydraulic evaluation conducted during the preparation of TM-1WQ
- To develop the hydraulic basis of design for further evaluation and development of the conceptual design of UV disinfection facilities
- To determine the need for a low lift pump station with the addition UV disinfection facilities both prior to and after the potential addition of tertiary filters

For the purposes of the Disinfection Cost Study, sound engineering judgment will be used to make assumptions regarding the most likely arrangement of the proposed facilities based on the current status of the future planned improvements to the SWRP.

In the following discussion, the results of this evaluation are given. The sections that follow summarize the determination of the process flow through the UV Disinfection Facilities, the hydraulic profile through the proposed UV Disinfection System, and the details of the Low Lift Pump Station.

2 PROPOSED FACILITIES

The proposed facilities considered in this study revolve around adding disinfection process facilities to the existing process train and all associated improvements required due to that addition. As such, the improvements would include a disinfection facility/building based on ultraviolet disinfection technology, additional effluent flow conduits and a new plant outfall, gate structures to redirect flow to the new facilities, and a low lift pump station. Tertiary filters would not be included, although the proposed disinfection facilities would be designed to allow the future addition of tertiary filters. The decision to proceed with UV technology for disinfection was made by the District based on several factors including track-record of the technology, the need to avoid release of additional chemicals to the environment such as chlorination byproducts, security concerns related to chlorine use and storage and the cost comparison between the short-listed disinfection technology alternatives (ultraviolet treatment and ozonation) performed as part of TM-1WQ. UV technology was shown to be less costly than ozonation with substantially less concern regarding byproducts and security compared to chlorination/dechlorination.

2.1 Key Considerations for Design Development

In order to further develop the design for the UV Disinfection Facilities, CTE has reviewed the basis for the decisions that were incorporated into TM-1WQ in order to confirm the validity of those decisions. This review has identified several issues that must be addressed during the conceptual design of the facilities.

2.1.1 Site Constraints

Proposed Treatment Train

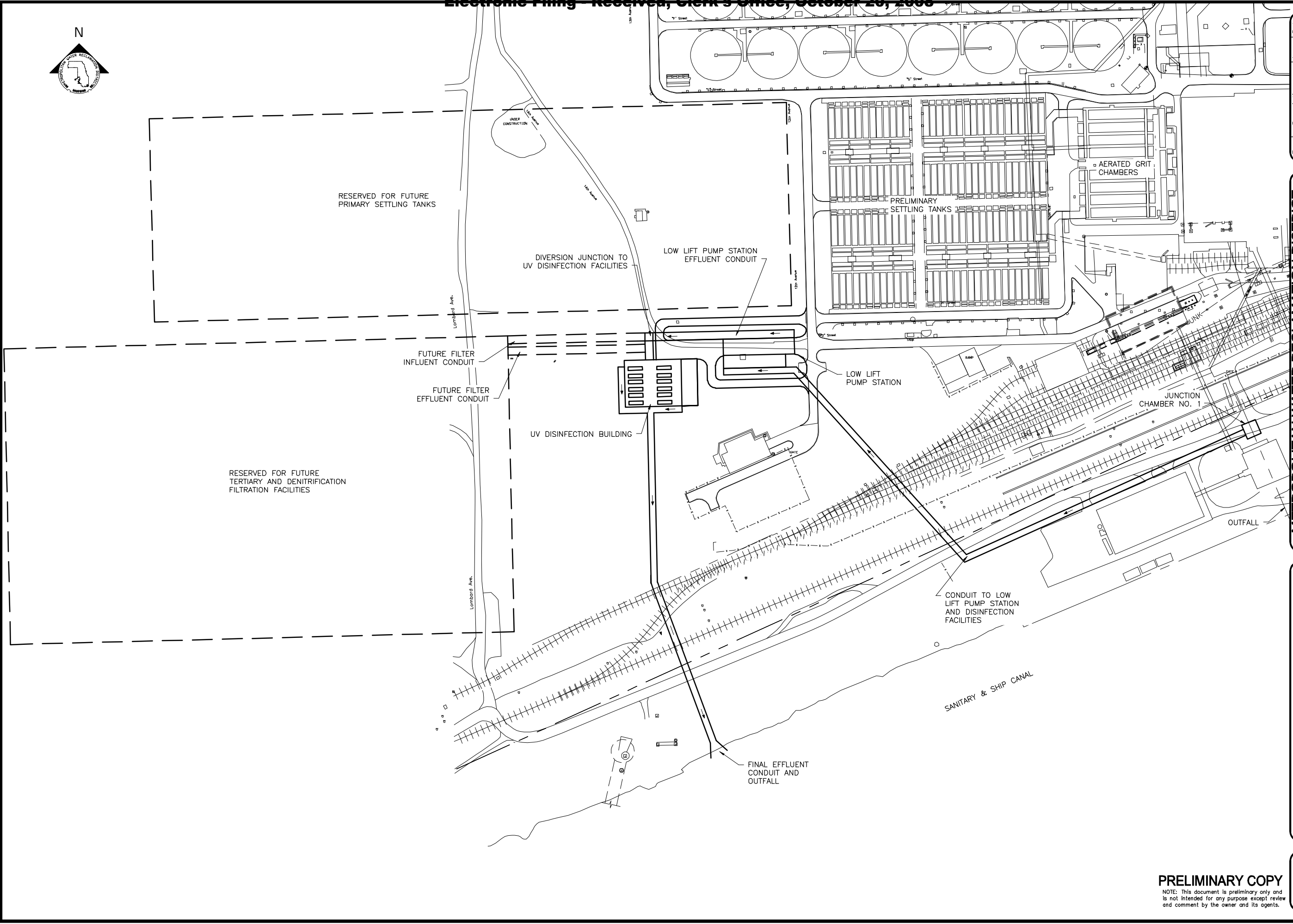
Disinfection facilities are usually located at the farthest possible downstream point in the process treatment train for the reason that the more treatment the effluent receives to remove both dissolved and suspended contaminants, the more effective the disinfection process.

One major change from TM-1WQ is the relaxation of the assumed need for tertiary filtration as part of the disinfection facilities. TM-1WQ presented scenarios with and without filtration based on the lack of information to demonstrate that filtration was not required for effective disinfection. For the purposes of this study, it is assumed that tertiary filtration would not be required in the near term. However, if tertiary filtration is implemented in the future, it would be beneficial for filtration to occur prior to disinfection to leverage the benefits of lower suspended solids and BOD concentrations that would make disinfection both more efficient and potentially allow the UV facilities to be downsized.

Space

Appendix A shows the proposed future site plan from the SWRP Master Plan as included in TM1-WQ. The TM1-WQ allocated space in the southwest area of the existing site for disinfection and tertiary filtration due to the amount of available open space and the relative proximity to the Ship and Sanitary Canal (SSC). However, this would require an extensive effluent conduit to convey flow from near the Pump and Blower Building nearly 1,500 LF to this location and a new effluent outfall into the SSC. Also, the majority of the space needs in this location are allocated to future tertiary filtration. The filter space allocated is based on denitrification media filtration at 1.5 gpm/sf. Although other filtration technologies are available with smaller space requirements, it is prudent at this time to assume denitrification filtration for planning purposes.

In consideration of these points, the location provided in TM-1WQ is recommended as it provides sufficient open space for the new facilities as well as provides flexibility for future implementation of tertiary filters is so required. The arrangement of the new facilities in the south-west area of the plant has been altered from TM-1WQ to provide for better usage of the site, as shown in **Figure 1**.



Rev.	Description	Appr.	Date

METROPOLITAN WATER RECLAMATION DISTRICT OF GREATER CHICAGO			
Designed by: XX	Checked by: XX	Correct: ENG	Approved: MWRD Assistant Chief Engineer
Drawn by: MB	Reviewed by: XX	Date: JUN 2008	Scale: 1:100

STICKNEY WATER RECLAMATION PLANT
CONTRACT 07-026-2P
 UV DISINFECTION COST STUDY
**SWRP
 SITE PLAN**

Sheet Number:
FIGURE 1
 Page Number: XX

PRELIMINARY COPY
NOTE: This document is preliminary only and is not intended for any purpose except review and comment by the owner and its agents.

2.1.2 Hydraulic Constraints/Need for Additional Pumping

The final key consideration for development of the potential disinfection facilities at SWRP is the hydraulic constraints that may limit the ability to convey flow through the facilities by gravity. CTE has completed hydraulic evaluations to estimate the headloss through the UV Disinfection Facilities including the required conduits to evaluate the ability to flow through the proposed facilities by gravity.

The flow through the SWRP is currently via gravity from Aeration Batteries A, B, C and D, underneath the Pump and Blower Building to the plant outfall discharging into the Ship and Sanitary Canal (SSC). The existing hydraulic condition was analyzed from the existing effluent aerator downstream of Battery B, as this represents a hydraulic break point, to the outfall in order to determine the head available for the disinfection facilities. CTE conducted this hydraulic evaluation based on three assumptions:

1. A water surface elevation (WSE) of 3.5 ft CCD in the SSC based on the hydraulic profile from the Contract 78-102-EP, West-Southwest Treatment Works, February, 1985¹ was used as the historical hydraulic basis of design for the existing facilities. This does not meet the 100-year flood requirements.
2. Secondary effluent to the new disinfection facilities would be diverted through a new junction chamber located just downstream of the Pump and Blower Building, at a point approximately 800-ft upstream of the outfall. At this location, secondary effluent from all Aeration Batteries (A, B, C & D) could be diverted to the new facilities.
3. Peak flow of 1,440 MGD was used to size the hydraulic conduits.

The difference between the water surface elevation at the Pump and Blower house and the historical water surface elevation in the SSC is the head available to convey flow through the new disinfection facilities by gravity. **Table 1** presents the results of that evaluation.

Table 1 - Theoretical Water Surface Elevation Assuming All Gravity Flow, Existing Conditions

Location	WSE
WSE just downstream of Pump and Blower House	5.45
WSE in SSC, taken from 1985 Hydraulic Profiles max water elevation	3.50
Available head, ft.	1.95

Note: All WSE in Chicago City Datum (CCD).

Per Table 1, only 1.95 ft of head is available to convey flow through the proposed disinfection facilities by gravity under previous hydraulic analysis conditions. Without tertiary filters, the headloss through the UV disinfection facilities, including associated flow splitting and control systems, is estimated to be 7.64 feet. Thus the available head is insufficient to direct flow through the potential disinfection facility by gravity alone.

¹El 3.5 ft CCD is listed as the water level in the Sanitary and Ship Canal for which the hydraulics were evaluated, based on a maximum design flow rate of 2,000 MGD. This profile appears to be the last official hydraulic profile conducted for the SWRP.

As a result, additional pumping would be required after the implementation of the UV disinfection facilities to meet the required peak flow rate of 1,440 MGD.

Considering that this is a conceptual level evaluation, additional headloss is possible and likely to be identified during final design as the details of flow splitting arrangements and other site constraints create less than ideal flow conditions.

3 HYDRAULIC ANALYSIS OF THE UV DISINFECTION FACILITIES

3.1 Objectives

Hydraulic analyses of the SWRP had not been performed as part of the Master Plan, thus the objective is to identify any possible hydraulic bottlenecks in the proposed disinfection facilities for the recommended site plan indicating where detailed analysis will be required during the design phase. For this study a preliminary model was created to evaluate the hydraulics following the addition of the UV Disinfection Facilities inclusive of the required addition effluent conduits, gate structures, UV channels and reactors and the Low Lift Pump Station (LLPS).

3.2 Overview

The hydraulic analysis was completed using a spreadsheet utilizing standard open channel and closed conduit flow equations to represent the SWRP from the effluent conduit at the Pump and Blower house through a new junction chamber to the new LLPS, through the new UV facility and discharged to the outfall. The hydraulics evaluated were for the year 2040 conditions, utilizing a peak flow of 1,440 MGD, which includes both infrastructure and permit-related improvements. The hydraulic analysis considered the existing plant hydraulics starting from the hydraulic break created by the effluent aerator, downstream of Battery B.

Although a WSE Elevation in the SSC of 3.5 ft CCD was utilized to determine if effluent pumping is required based on the historical hydraulic basis of design, the 100-year flood elevation for the Sanitary and Ship Canal has been calculated using the USACE's Chicago Underflow Plan (CUP) Design Report. The CUP report used observed high water levels to model the predicted high water levels throughout the Chicago Area Waterways at each of the construction phases. The observed high water level at the SWRP outfall is approximately 4.1 ft CCD (since 1965) and the peak modeled level for the 1957 event (estimated at greater than the 100-year flood) is 10.1 ft CCD. Appendix B provides select pages from this report.

From the CUP report, a water surface elevation of 9.0 ft CCD was estimated at the SWRP outfall for the 100-year flood. For the conceptual design of the new UV facilities in this study, the water surface elevation of 9.0 ft CCD will be utilized as a worst case hydraulic constraint in order to ensure the new facilities can operate during the 100-year flood.

3.3 Assumptions

Due to the preliminary nature of the selected site plan, assumptions were made in the development of the hydraulic model. These assumptions are as follows:

1. Peak flow of 1,440 MGD. Flows above 1,440 MGD are diverted to the TARP system.

2. SWRP drawings obtained from MWRDGC are on the Chicago City Datum (CCD) or the National Geodetic Vertical Datum (NGVD). All elevations were converted to CCD using conversion $CCD = NGVD - 579.48$.
3. The CCD has not changed since the plant was originally constructed in the 1920's.
4. The estimated 100-yr flood elevation is +9.00 CCD, as calculated in the Chicago Canal System Model, UNET. Appendix B provides selected pages from the USACE's Chicago Underflow Plan (CUP) Design Report presenting these results. Pre-Stage 1 (Stage 1 of the McCook Reservoir Construction) values are used since the USACE's current estimate for completion of Stage 1 construction in 2020 or later.
5. Post Aeration is not included in this study. Additional headloss and costs would be associated with the inclusion of post-aeration.
6. Velocity in Disinfection Influent and Effluent Distribution Chambers is zero to allow adequate flow distribution.
7. Batteries A, B, C and D are all at the same elevation and flow is equally divided between the Batteries A, B, C and D, with each receiving 360 MGD.
8. The UV process requires approximately 6 ft of submergence, thus the disinfection channel effluent weir is assumed to be 5.5 ft above invert to ensure a submerged weir at low flow conditions.
9. The following modeling equations were used:
 - a. Pressure Flow – Hazen Williams Equation
 - b. Open-Channel Flow – Manning's Equation
 - c. Flow junctions – Pressure Momentum Analysis
10. Hydraulic coefficients used in developing this model include:
 - a. Hazen Williams – 110 (concrete)
 - b. Manning's
 - i. Regular channel – 0.013
 - ii. Aerated channel – 0.035

3.4 Results

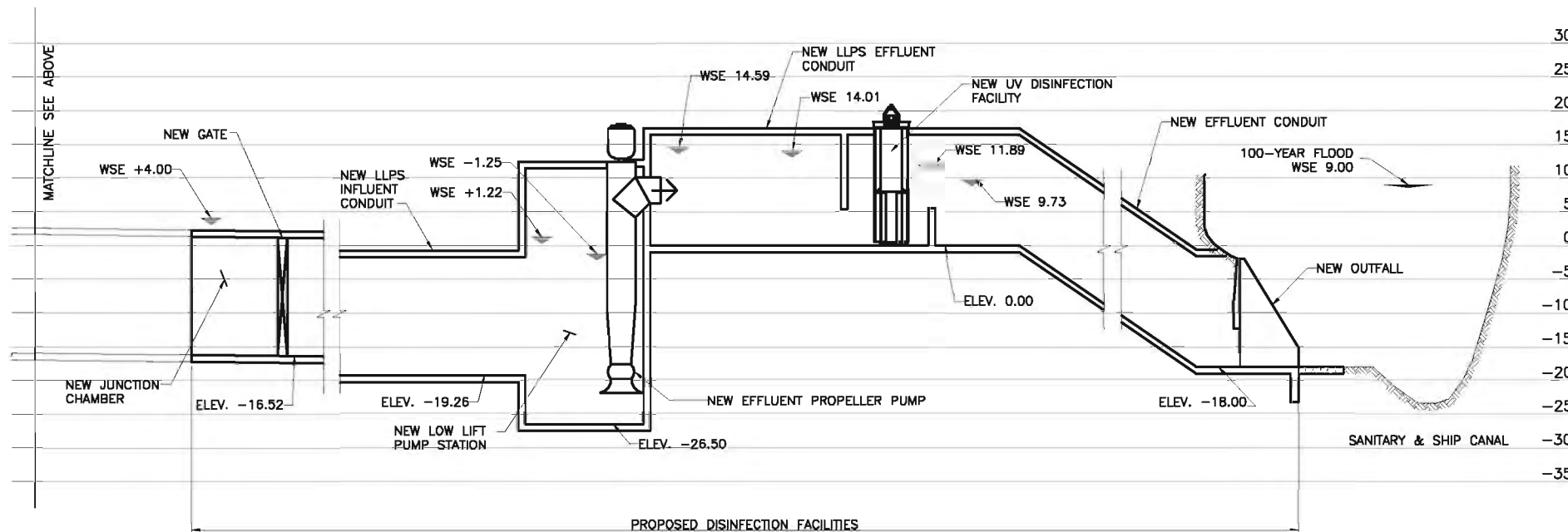
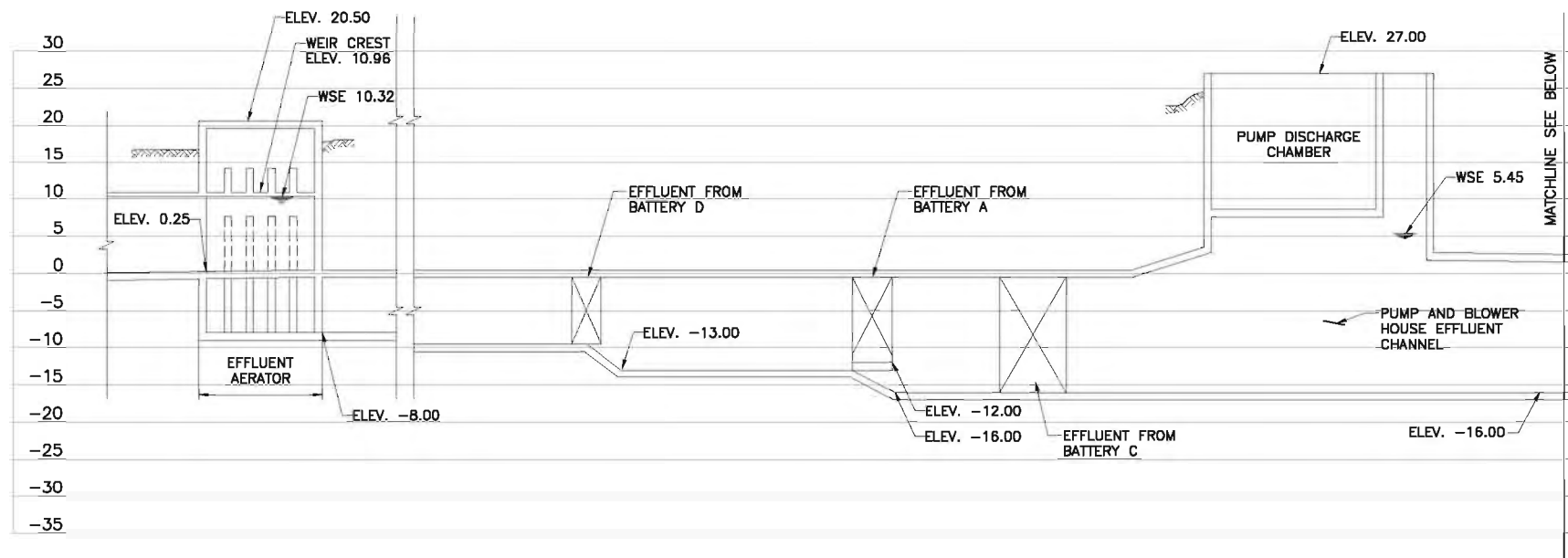
The results of the hydraulic analysis are presented in **Table 2**. Table 2 presents the estimated water surface elevations through the plant from the existing Effluent Aerator through the new LLPS and UV Disinfection Building and to the new outfall.

The flow path starts with a new effluent conduit that would direct secondary effluent by gravity approximately 1,500 ft west from the new junction chamber near the Pump and Blower Building to the new LLPS. Flow would then be lifted 15.8 ft to the new UV influent conduit. Flow would travel by gravity through the UV facilities, which would be split into two banks of six UV reactors, into an effluent conduit and to a new outfall discharging into the SSC.

Table 2 - Summary of Proposed WSE including UV Disinfection Facilities

Location	WSE
Effluent Aerator Discharge Weir Elevation	10.96
WSE in Effluent Aerator	10.32
WSE just downstream of Pump and Blower House	5.45
WSE at New Junction Chamber	4.00
WSE in LLPS Influent Conduit	1.22
WSE in LLPS Wet Well just u/s of curtain wall	-1.25
WSE just downstream of Low Lift PS	14.59
WSE just upstream of Influent gate	14.01
WSE just upstream of Effluent Weir gate	11.89
WSE at downstream of Disinfection Effluent Chamber	9.73
WSE in Sanitary and Ship Canal, Approximate 100 yr flood elevation	9.00

The estimated water service elevation at the existing effluent aerator remains below the existing aerator weir elevation, thus maintaining the existing hydraulic break. **Figure 2** contains the hydraulic profile of the flow path through the proposed UV disinfection facilities and the available freeboard at the locations where water surface elevations (WSE's) were calculated at the maximum day flow.



PLOT DATE: 6/2/2008 9:42 AM PLOTTED BY: WORTH, SELINA

Rev.	Description	Appr.	Date

METROPOLITAN WATER RECLAMATION DISTRICT OF GREATER CHICAGO		Approved by: MWRD Assistant Chief Engineer
		Checked by: Correct Designed by: XX
Drawn by: LK	Reviewed by: XX	CTE AECOM
Date: 1/2008	Scale: NTS	CTE AECOM <small>500 East Wacker Drive, Suite 600, Chicago, Illinois 60601-2278 T 312.850.0000 F 312.850.1100 www.aecom.com</small>

CONTRACT 07-026-2P
 STICKNEY WATER RECLAMATION PLANT
 ULTRAVIOLET DISINFECTION FACILITIES
 PROPOSED HYDRAULIC PROFILE
 DISINFECTION FACILITIES

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FIGURE 2
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4 UV DISINFECTION FACILITIES

The District has preliminarily selected the medium-pressure high-intensity (MP-HI) UV disinfection technology for potential disinfection of final effluent at its water reclamation plants. This section presents the preliminary basis of design of the UV system to be used at the SWRP.

4.1 Background

A Technical Memorandum on the UV Disinfection Technology was completed for the North Side WRP UV Disinfection Cost Study. The memorandum incorporated the following information which is relevant to the Stickney WRP:

- Information from literature including technical proceedings from the Water Environment Federation (WEF), Water Environment Research Foundation (WERF), proceedings from the latest Disinfection conference series undertaken by WEF, American Water Works Association (AWWA), and International Water Association (IWA). This information provided the latest updates in the UV disinfection technology.
- Updated recommendations on the UV system from four manufacturers – Trojan Technologies, Aquionics, Calgon Carbon, and Severn Trent Services (STS)/Quay.
- Reference information on experience of UV disinfection at five selected facilities – Racine WWTP (Racine, WI), R.L. Sutton WRF (Cobb County, GA), Grand Rapids WWTP (Grand Rapids, MI), Jacksonville WWTP (Buckman, FL), and Valley Creek WWTP (Valley Creek, AL). A summary of important inferences from the phone survey are as follows.
 1. Fouling due to iron in the effluent has been a problem at the Racine, Sutton, and Grand Rapids facilities. Fouling results in lower than expected disinfection performance, higher operating costs, and higher M&O efforts. The iron in the effluent at all three plants was primarily from the chemical phosphorus removal using Ferric Chloride. At Grand Rapids WWTP, the chemical addition is upstream of the secondary treatment process; staining of sleeves was found only when the chemical addition was in the secondary clarifiers. At the Sutton WRF, fouling of lamps due to iron is observed although chemical addition is upstream of secondary process and sand filters are used upstream of the UV disinfection system. At the Racine WWTP, fouling may be due to ferric chloride addition and/or due to the additional iron brought by the ferric sludge from another water treatment plant, although operational controls are used to prevent both sources from occurring simultaneously.
 2. Calcium fouling due to hardness in the source water is not a significant problem because of the automatic mechanical/chemical cleaning system that dissolves and wipes away any scales. The lack of calcium hardness was observed in all five plants including the Racine and Grand Rapids utilities which have Lake Michigan source water and is attributed to the automatic cleaning system performance.
 3. The frequency of cleaning and changing of the cleaning solution is specific to the utility and would have to be determined only by experience; however it is likely to be more than the typical case stated in the literature.

4. Labor requirements varied amongst facilities, with some facilities requiring more labor to handle the fouling caused by iron salt addition.
5. As long as other processes in the plant are performing as desired, all five facilities were satisfied with the UV disinfection system because it met their disinfection goals.

In conclusion, the phone survey had revealed that fouling of the quartz sleeves is a concern for this application, particularly if iron salts are added for phosphorous removal in the future. In addition, the phone survey results suggest that the manufacturer's recommended labor assumptions for routine maintenance including cleaning and inspection of the lamps is too low for this application. As transmissivity is directly related to lamp fouling, additional lamps and/or more frequent cleaning may be required in the future if iron salts are to be utilized in processes upstream of this technology.

Using this information and the updated information available from manufacturers, a preliminary basis of design of the MP-HI UV disinfection system has been developed for disinfection of the final effluent at the SWRP.

4.2 Basis of Design

The MP-HI system involves sending the secondary or tertiary effluent through channels containing banks of MP-HI UV lamps. The Trojan UV4000™Plus system is used here to develop the basis of design for the UV disinfection system. The system consists of a power supply, an electrical system, a reactor, MP-HI lamps, a mechanical and chemical cleaning system, and a control system. The MP-HI UV lamps are enclosed in individual quartz sleeves for protection against dirt and breakage. Reactor chambers (open channels) hold the lamps in a horizontal configuration. The effluent weirs and level sensors are used to keep the lamps submerged under the effluent water. This submergence ensures that the lamps do not overheat, thereby preventing lamp life reduction or burnout.

The UV system is assumed to operate from March to November each year. During the winter months, the equipment would sit idle as the flow is bypassed around the LLPS and UV Disinfection Building. However, due to the size of the facility including twelve reactors and over 4000 lamps, maintenance activities would be conducted every working day from March to November and periodically during the winter months. It is reasonable to expect that the area would continue to experience normal weather patterns for the Chicago area including extreme weather during all four seasons. In order to protect the safety of the M&O staff, ensure operational and maintenance-related productivity, and protect the UV equipment from adverse weather common to the Chicago area including high winds, rain, lightning, snow, and extreme temperatures, the UV system would be enclosed in a building.

4.2.1 Proposed Design Criteria for UV Disinfection Equipment

Based on a review of the information provided by the UV equipment manufacturers and the experience of five other facilities, it is observed that Trojan Technologies provides a widely-used low-maintenance solution for final effluent disinfection. The design of the MP-HI UV disinfection system for the SWRP is based on the Trojan UV4000™Plus equipment provided by Trojan Technologies.

4.2.2 Proposed Layout

Flow would enter the UV disinfection facilities at the north end of the influent chamber, where it would be directed east and west through 72-inch gates through two (2) banks of six (6) UV channels arranged on either side of the influent chamber. The effluent channels combine the flow to the south of the UV building and direct it to a new outfall. This layout provides for a compact site footprint and the enables the building size to be minimized.

The conceptual layout provides for a new effluent outfall to the SSC, rather than directing the disinfected effluent back to the existing outfall. However, it is likely that the construction of a new outfall would require permitting and an environmental impact assessment which may eliminate this option and necessitate the existing outfall being used during final design.

4.2.3 Proposed Basis of Design Criteria

The basis of design is given in **Table 3**.

Table 3 – Design Parameters for UV Disinfection Unit at NSWRP

Parameter	Design Value
Capacity and Water Quality	
Design flow, mgd	1,440
Average flow, mgd	1,250
Maximum TSS ^a , mg/L	15
Pre-Disinfection Effluent E.Coli Count ^b , cfu/100 mL, maximum (Assumed)	200,000
Post-Disinfection Effluent E.Coli Count Target ^c , cfu/100 mL	400
Effluent Hardness ^d , mg/L as CaCO ₃	270
Dosage	
UV transmittance, minimum, %	65
UV intensity ^e , W/lamp	4,000
Lamp Life, hours	5,000
Fouling factor, %	90
Lamp aging factor, %	89
UV dose, mW-s/cm ²	40
Physical Characteristics	
Channel dimensions, WxD	106" x 172"
Number of channels	12 (11 plus 1 standby)
Number of reactors per channel	1
Number of banks per reactor	2
Number of modules per bank	7
Number of lamps per module	24
Total number of lamps	4,032
Total power requirement, kW	11,827
Average power requirement, kW	9,225
Hydraulics	
Headloss, UV reactor only	9"
Velocity in each channel, V, ft/s	1.87
Liquid level control in channel	Motorized Weir Gate

^a Monthly permit limit 12 mg/L

^b Annual average

^c Future requirement (monthly geometric average)

^d Mean value

^e 100% intensity at 100 hours of lamp use

The above design criteria are assumed based on available information and the current state of ultraviolet disinfection technology. A more extensive technology evaluation

should be conducted prior to final design of the facility. Due to the extraordinary scale of this facility, CTE recommends the District undertake the following design process for selection and design of the UV disinfection equipment if final design is initiated:

1. Request and evaluate independent, full-scale validation data (also known as biosimetry data) from manufacturers of candidate disinfection systems for similarly sized units or the largest size for which the manufacturer has data available. This evaluation would provide an initial level-of-confidence that the candidate systems can achieve the target disinfection levels. Data should be from systems using the same bulb, ballast, and control technology as proposed for the full-scale system.
2. Conduct a collimated beam testing program. This program would use site specific effluent and bacteria to determine the sensitivity of the site specific bacteria and pathogens to UV disinfection. The data would be used to size the UV lamps and reactors.
3. Increase frequency of UV transmittance testing at each plant to at least once per day for a period of one year or more to collect data on seasonal variability, daily variability, diurnal variability, and to capture the frequency of events that might reduce transmissivity such as wet weather and infrequent industrial discharges.
4. Conduct a more detailed life cycle cost analysis of the candidate disinfection systems based on the data collected during steps 1 through 3 above.
5. Construct a pilot testing facility designed to match lamp spacing, velocity profile and other design parameters of the proposed full scale units. The pilot testing facility would be used to determine:
 - a. Appropriate control sequences and optimization for the UV disinfection equipment, including appropriate sensing equipment to allow advanced power management.
 - b. In-situ disinfection performance including fouling rates of the lamps with and without ferric salt addition.
 - c. Design life of lamps and other UV system parts.
 - d. Actual M&O requirements in terms of labor and consumables as well as space requirements to complete required maintenance activities.
 - e. Performance of alternate equipment manufacturers, if alternates are available at the time of piloting.
 - f. Accuracy of life cycle cost analysis prior to final design of the full-scale system.
6. Conduct post-construction full-scale validation testing (biosimetry testing) to confirm performance and determine operating parameters.

Using a program as described above, it may be possible to demonstrate the effective UV dosages to the regulators and optimize the equipment sizing criteria. For this study, reduction in the Illinois requirements for UV system sizing is not assumed based on the lack of data similar to that described above.

5 LOW LIFT PUMP STATION

This section will present the proposed arrangement and key characteristics of the proposed Low Lift Pump Station.

5.1 Pump Type

Several pump types were considered for this application. Pump types considered included screw pumps, vertical turbine pumps, centrifugal pumps, and axial flow pumps. Screw pumps and axial flow pumps appear to have the best operating performance for this condition.

It is estimated that the low lift pumps would lift 1,440 MGD of secondary effluent approximately 22.3 feet (TDH) to the UV disinfection system influent, including estimated head to allow flow through the UV system. The static head equates to the difference in the estimated water surface elevation between the wet well and the discharge conduit plus an additional 2-ft of head added as a conservative factor to accommodate additional losses that may be identified during final design.

If tertiary filtration is constructed in the future, the TDH would most likely increase but the flow would remain the same. Screw pumps will not easily accommodate this change in head, without significant structural modifications to the pump station. However, axial pumps can be modified for future head conditions. Structural modifications to the pump station to accommodate these changes, if required, should be minimal. Therefore, axial flow, propeller type pumps are recommended.

Vertical axial flow pumps have been assumed here, but other configurations (including inclined or horizontal) could be considered in the future.

5.2 Basis of Design

Table 4 provides a summary of the basis of design for the Low Lift Pump Station.

Table 4 - Low Lift Pump Station Basis of Design

Flow, MGD	1,440
Pumps	
Type	Axial Flow
Number	8 total (N+1+1)
Pumping Rates, gpm/pump	166,670
Static Head, ft	15.8
Dynamic Head (inc. station losses), ft.	4.5
Total Dynamic Head, ft. ⁽¹⁾	22.3
Motor, hp ⁽²⁾	1,500
Suction Head, ft	18.5
Wet Well	
Length, ft.	86
Width, ft.	114

(1) The static head equates to the difference in the estimated water surface elevation between the wet well and the discharge conduit plus an additional 2-ft of head added as a conservative factor to accommodate additional losses that may be identified during final design.

(2) A 1,350 hp motor could be provided, however this is a non-standard motor size and only standard motor sizes were assumed for this conceptual study.

5.3 Proposed Operational Description

The pump station would have a total of eight pumps, with six duty pumps, one standby and one out of service (N+1+1). Five pumps would be driven by constant speed motors, three would be variable speed driven. In order to provide operational flexibility, the pump station would be divided into two wet wells, each containing four pumps. Design average flow (1,250 MGD) would be handled by four constant speed and two variable speed pumps operating at reduced speed, leaving two pumps on standby. Peak flow (1,440 MGD) would be handled by six pumps operating at full speed, leaving two on standby.

The pumps would operate 24 hours a day, seven days per week. Typically, at least one variable speed pump would operate at all times, to handle fluctuations in flow. **Table 5** illustrates an example of pump operation at design average flow and peak flow:

Table 5 - Summary of Pump Operation

Flow, MGD	Pump Drive Type	Pump Flow, gpm
700	Constant speed	166,667
	Constant speed	166,667
	Variable speed	152,777
1250 (Design Average)	Constant speed	166,667
	Constant speed	166,667
	Constant speed	166,667
	Constant speed	166,667
	Variable speed	100,694
	Variable speed	100,694
1440 (Peak)	Constant speed	166,667
	Constant speed	166,667
	Constant speed	166,667
	Constant speed	166,667
	Constant speed	166,667
	Constant speed	166,667
	Variable speed	166,667

In order to eliminate vortices, pumps require a minimum submergence as a function of pump suction bell diameter. For this flow condition, a 120-inch suction bell is required, which requires a minimum submergence of 16 feet. Submergence requirements should be verified by the pump manufacturer during final design.

Level sensors in the wet well would relay signals to turn pumps on and off. The level control would be automatic under normal conditions, with manual override possible. Other control inputs that need to be monitored include discharge pipe pressure, flap gate position, and motor alarms.

5.4 Proposed Layout

Flow would enter the pump station at the south end of the wet well, where it would be directed perpendicularly to the north through eight 96-inch slide gates. Pumps are

located at the north end of the pump station. Site constraints and pump station size appear to make this flow pattern necessary. Due to the excessively large area needed to meet Hydraulic Institute (HI) Standards, there is insufficient area available to meet the suggested dimensions directly.

A rectangular wet well is shown in the plan and section. Design features, which have been shown to be effective in other installations, were incorporated in this design in order to meet HI standards. For example, perforated plates, curtain walls, and floor and back wall splitters have been incorporated into the conceptual design. (See Appendix C for a plan and section of the proposed layout). Sizing and details of these types of features are normally determined by physical scale modeling during detailed design.

6 SUMMARY

A review of TM-1WQ confirms that the disinfection facilities would consist of UV technology without requiring tertiary filters, although filtration could potentially reduce the size of the UV facility via reductions in TSS and BOD. Additionally, the disinfection facilities are recommended to be located in the southwest corner of the existing site, adjacent to the space reserved for the future tertiary filters. In order to direct flow to the proposed location, a new junction chamber would be constructed just upstream of the existing outfall to divert flow to the new disinfection facility. It would also permit bypassing of the disinfection facility during winter months when disinfection is not required.

A hydraulic basis of design was developed for a peak plant flow of 1,440 MGD. This preliminary evaluation indicated that additional pumping would be required to lift secondary effluent up approximately 16-ft in order to flow through the proposed UV system. Axial flow pumps are recommended for the LLPS due to the low head conditions and the need to modify the discharge head when tertiary filters are added in the future.

Hydraulics were estimated starting from the existing effluent aerator, through the LLPS and UV facilities, and ending at a new outfall to the SSC.

The proposed conceptual layout of the new UV facilities consists of the following:

- a. Junction chamber with isolation gates within the existing plant effluent conduit and an conduit to the LLPS,
- b. LLPS:
 - i. Building housing a wet well and eight (8) axial flow pumps.
 - ii. Influent and effluent conduits with isolation gates.
 - iii. Support facilities such as an operator and storage rooms.
- c. UV Facility
 - i. Building housing twelve (12) UV reactor channels.
 - ii. Influent and effluent channels with isolation and level control gates.
 - iii. Support facilities such as an operator room, storage room and an electrical room housing the switchgear and transformers for both the LLPS and the UV facilities.

- d. A new effluent outfall to the Ship and Sanitary Canal.

The location and arrangement of these facilities was determined to accommodate future facilities as well as have functionality up to the 100-year flood elevation. A new effluent outfall is proposed, however permitting requirements may require this options to be reevaluated during final design

In conclusion, this review has confirmed the primary assumptions of the TM-1WQ in regards to the need for a low lift pump station, location of the facilities and arrangement of the facilities to accommodate future facilities.

APPENDIX A
Site Plan from the SWRP Master Plan

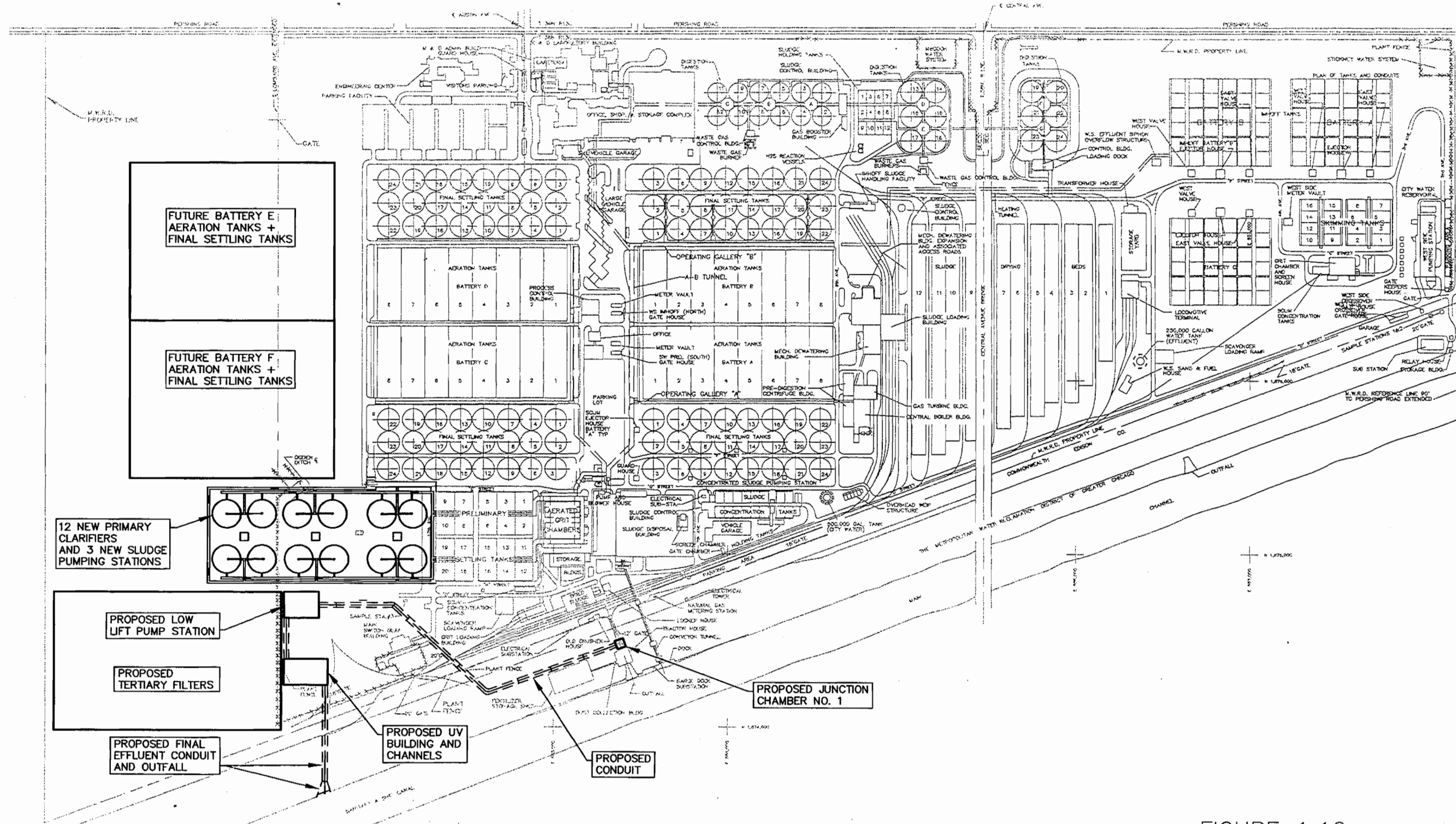
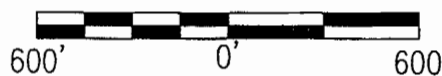
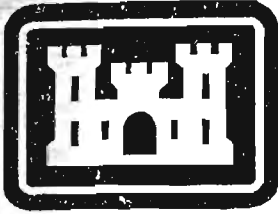


FIGURE 1.10
 SITE PLAN - UV DISINFECTION
 STICKNEY WATER RECLAMATION PLANT



APPENDIX B
Selected Pages from USACE CUP DDR



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CHICAGO DISTRICT

DESIGN DOCUMENTATION REPORT

**CHICAGOLAND UNDERFLOW PLAN
McCOOK RESERVOIR, ILLINOIS**

Volume I of VIII

NOVEMBER 1999



Table A-11. Canal System Observed and Modeled Maximum Water Surface Elevations

Location	Approx. River Mile	Maximum Water Surface Elevation (ft NGVD)						
		Observed, 1965 to present (Date)	Modeled for Water Years 1951-1988			Modeled 1% Chance Exceedance Event		
			Existing (Date)	Stage 1 Project (Date)	Stage 2 Project (Date)	Existing	Stage 1 Project	Stage 2 Project
Wilnette - NSC @ Sheridan Rd.	341.2	586.7 (4/18/75)	592.6 (7/57)	591.3 (7/57)	590.5 (7/57)	589.4	589.1	587.6
North Side SW - NSC @ Howard St.	336.8	588.4 (8/14/87)	594.9 (7/57)	593.1 (7/57)	592.6 (7/57)	591.8	590.9	589.5
North Branch PS - NSC @ Lawrence St.	333.0	588.8 (8/16/97)	594.6 (7/57)	592.2 (7/57)	592.2 (7/57)	591.7	589.8	588.4
Chicago River Controlling Works - Chicago River @ Lk Michigan*	325.6	583.6 (8/16/97)	589.1 (7/57)	585.3 (10/54)	583.9 (10/54)	588.2	585.0	583.2
31st & Western - CS&SC @ Willow Springs Rd.	320.5	583.6 (6/30/77)	589.6 (7/57)	585.4 (10/54)	583.9 (10/54)	588.7	585.1	583.0
Willow Springs - CS&SC @ Willow Springs Rd.	307.9	582.7 (7/18/96)	587.2 (7/57)	584.0 (10/54)	583.0 (10/54)	586.7	584.1	582.4
Sag Junction - Confluence of CS&SC and CSC	304.2	582.2 (7/18/96)	585.0 (7/57)	582.6 (10/54)	581.9 (10/54)	584.7	582.8	581.6
O'Brien Lock - Calumet River Downstream (south) of O'Brien Lock	325.8	583.8 (7/18/96)	585.0 (7/57)	584.6 (7/57)	584.6 (7/57)	584.7	584.0	583.8
Southwest Highway - CSC @ Southwest Hwy	310.8	583.7 (7/18/96)	585.0 (7/57)	584.3 (10/54)	584.3 (10/54)	585.0	583.5	583.1

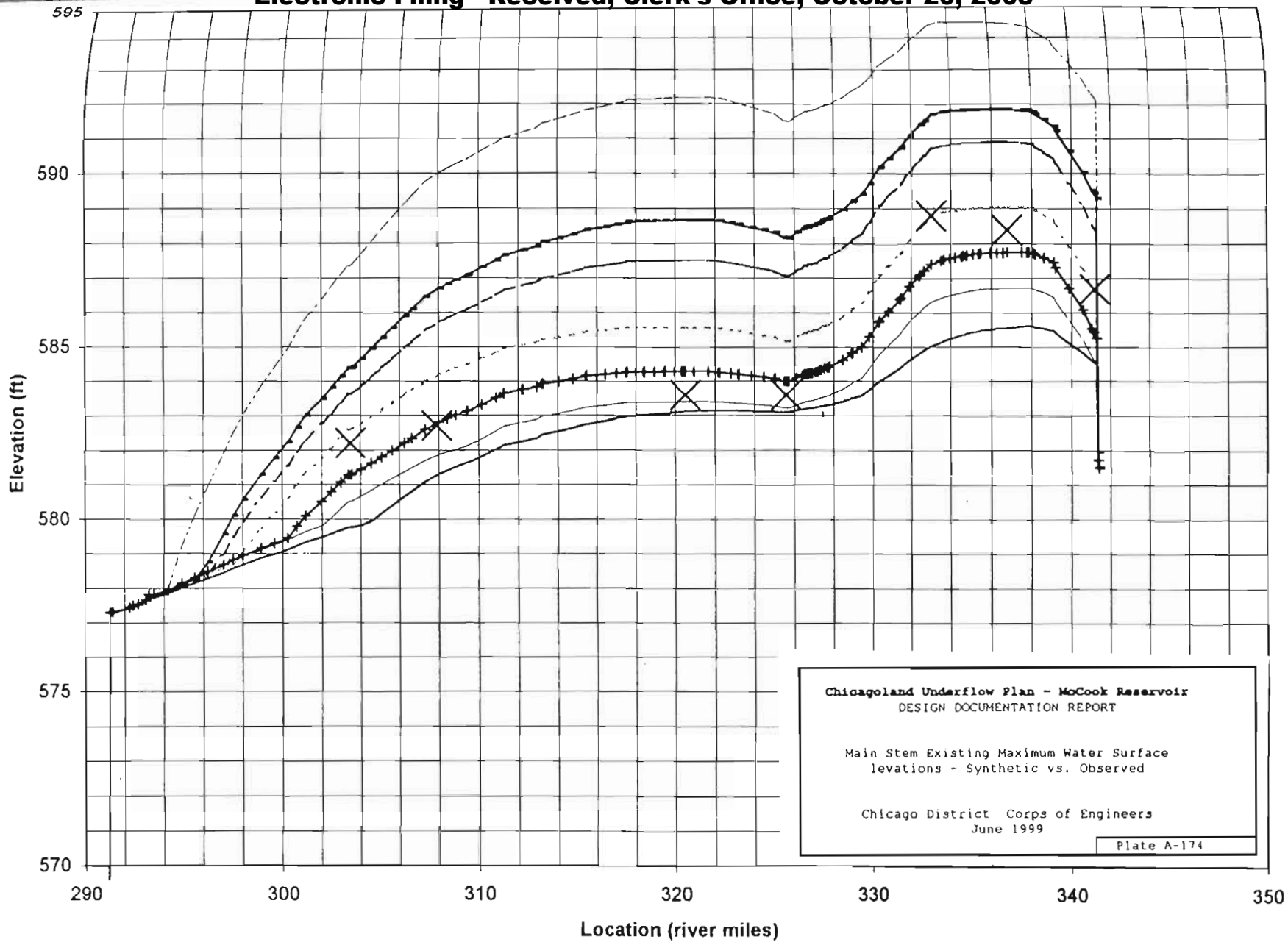
*The approximated river mile is for the junction of the Chicago River and its North and South Branch.

NSC = North Shore Channel
 CS&SC = Chicago Sanitary and Ship Canal
 CSC = Calumet Sag Channel

A-20

Table A-12. Index of Major Bridges and Confluences for Chicago Canal Model

Reach Scheme (Canal Model)	Tributary Stream	Bridge Name	River Mile
2	North Shore Channel	Sheridan Road Lock	341.2 1/
2	"	Central Street	340.4
2	"	Green Bay Road	339.8
2	"	Church Street	338.7
2	"	Demoster, Il 58	338.2
2	"	Oakton Street	337.2
2	"	Touhy Avenue	336.2
2	"	Devon Avenue	335.2
2	"	Peterson, US 14	334.7
2	"	Foster Avenue	333.6
2	"	Jct. North Branch	333.5
1	North Branch	Touhy	51.4 2/
1	"	(05536000 gage)	
1	"	Devon Avenue	49.2
1	"	Edens Expwy.	46.2
1	"	Cicero Avenue	46.1
1	"	Foster Avenue	44.5
1	"	Kimball Avenue	43.9
1	"	Kedzie Avenue	43.6
1	"	Jct. North Shore Channel	43.3
3	"	Jct. North Shore Channel	333.5
3	"	Lawrence Ave.	333.1
3	"	Montrose Ave.	332.5
3	"	Irving Park Rd.	332.0
3	"	Addison Street	331.4
3	"	Belmont Ave.	330.9
3	"	Western Ave.	330.6
3	"	Diversy Ave.	330.2
3	"	Damen Ave.	329.9
3	"	Fullerton Ave.	329.5
3	"	Ashland Ave.	329.1
3	"	Cortland Street	328.6
3	"	North Ave.	327.9
4	North Br. (Goose Island West)	Division Street	327.4
4	"	Ogden Ave.	326.9
4	"	Halsted Street	326.6
5	North Br. (Goose Island East)	Division Street	327.0
5	"	Ogden Ave.	326.9
5	"	Halsted Street	326.85
6	North Branch	Chicago Ave.	326.4
6	"	Ohio/Kennedy Expwy.	326.1
6	"	Grand Ave.	326.0
6	"	Kinzie Street	325.8
6	"	Jct. South Branch	325.6
7	Chicago River	Franklin Street	325.65
7	"	Wells Street	325.7
7	"	LaSalle Street	325.8
7	"	Clark Street	325.9
7	"	Dearborn Street	326.0
7	"	State Street	326.1
7	"	Wabash Ave.	326.3
7	"	Michigan Ave.	326.4
7	"	Lake Shore Drive	326.9
8	South Branch	Lake Street	325.6
8	"	Randolph Street	325.5
8	"	Washington Street	325.4
8	"	Madison Street	325.3
8	"	Monroe Street	325.1
8	"	Adams Street	325.0



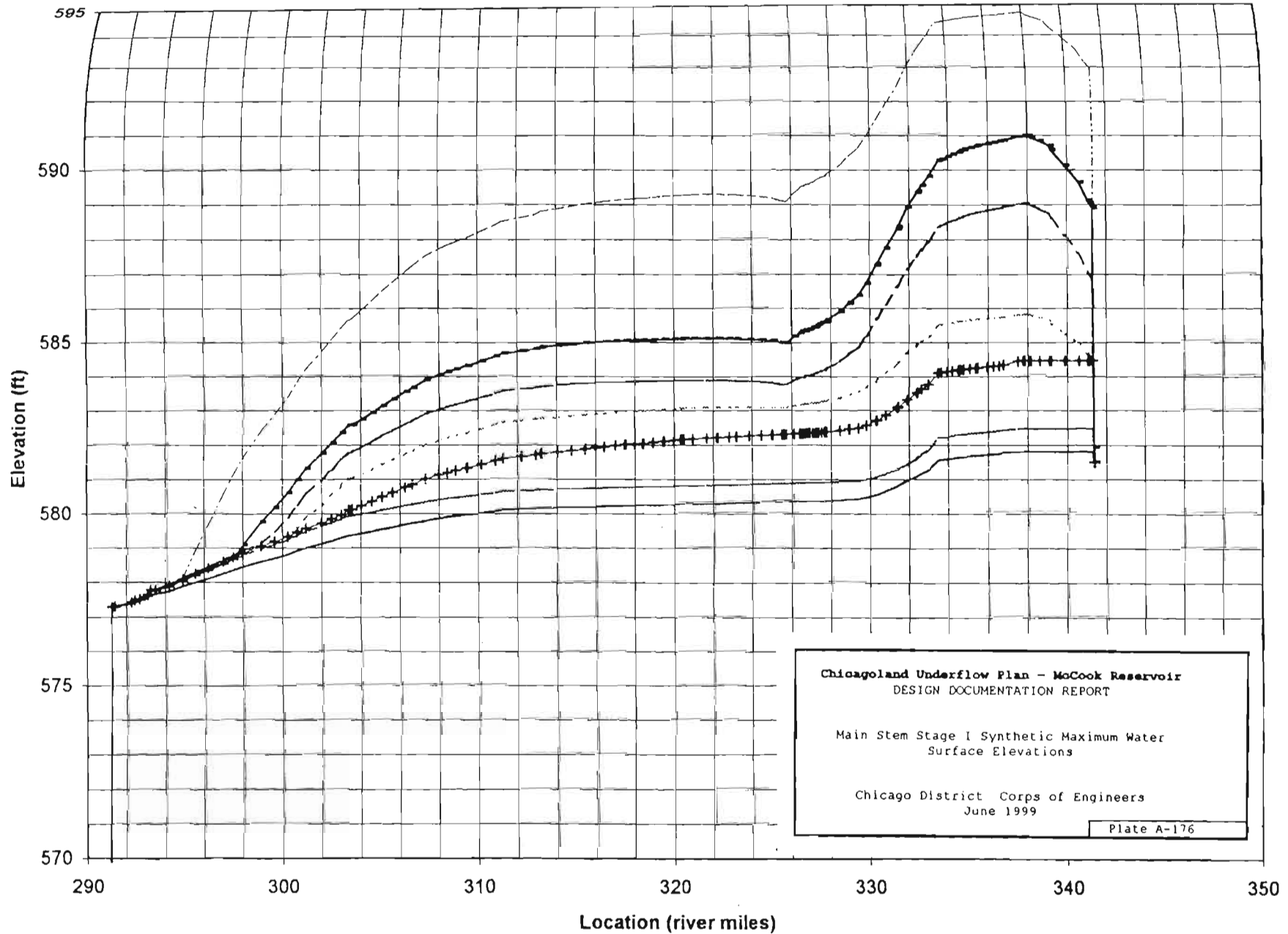
Chicago and Underflow Plan - McCook Reservoir
DESIGN DOCUMENTATION REPORT

Main Stem Existing Maximum Water Surface
Elevations - Synthetic vs. Observed

Chicago District Corps of Engineers
June 1999

Plate A-174

— 2-year — 5-year —+— 10-year - - - 20-year - - - 50-year — 100-year - - - 500-year X Observed High Water



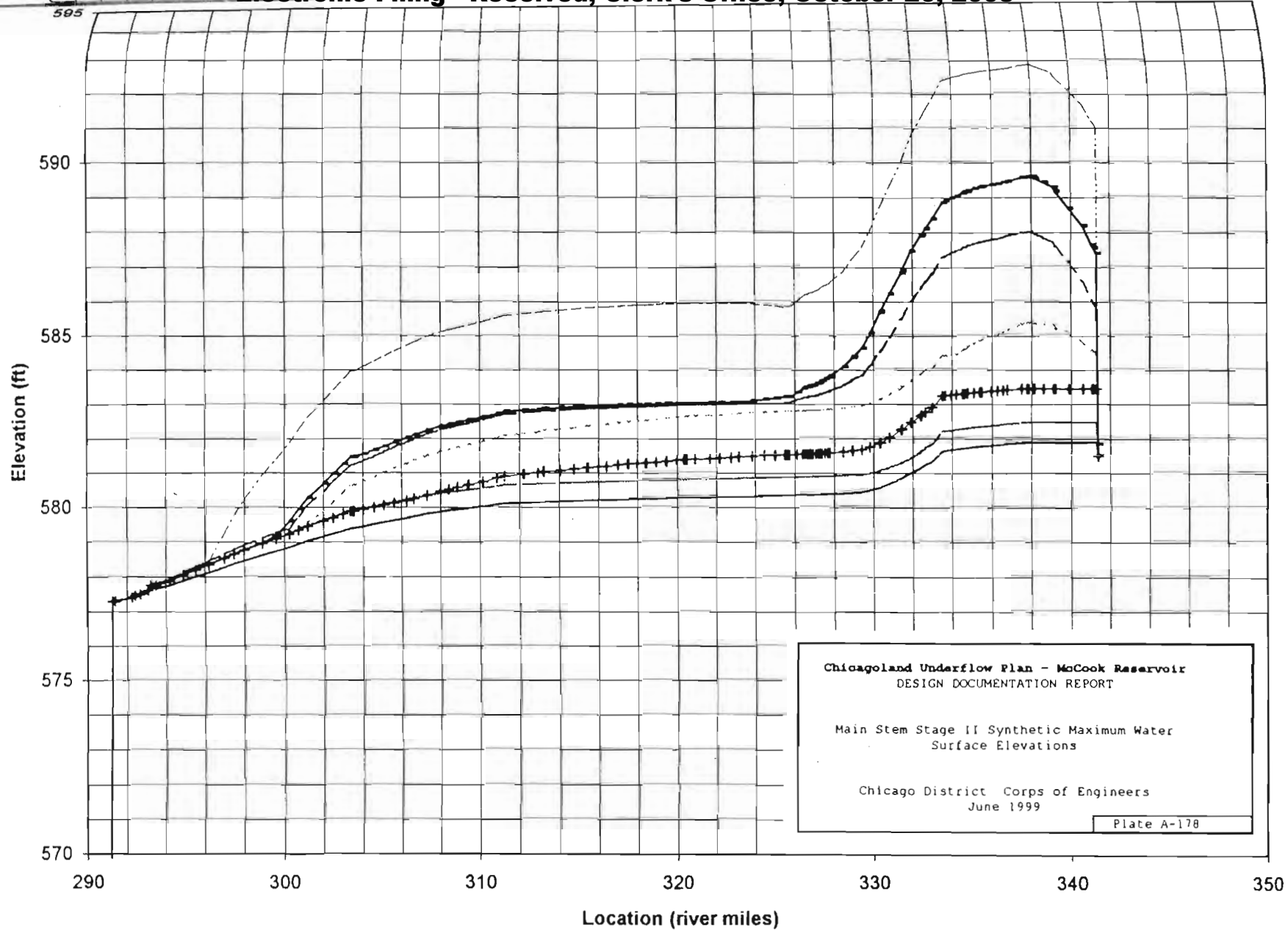
Chicago and Underflow Plan - McCook Reservoir
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Main Stem Stage I Synthetic Maximum Water
Surface Elevations

Chicago District Corps of Engineers
June 1999

Plate A-176

— 2-year - - - 5-year + 10-year ····· 20-year - · - · 50-year — 100-year - - - - 500-year



Chicagoland Underflow Plan - McCook Reservoir
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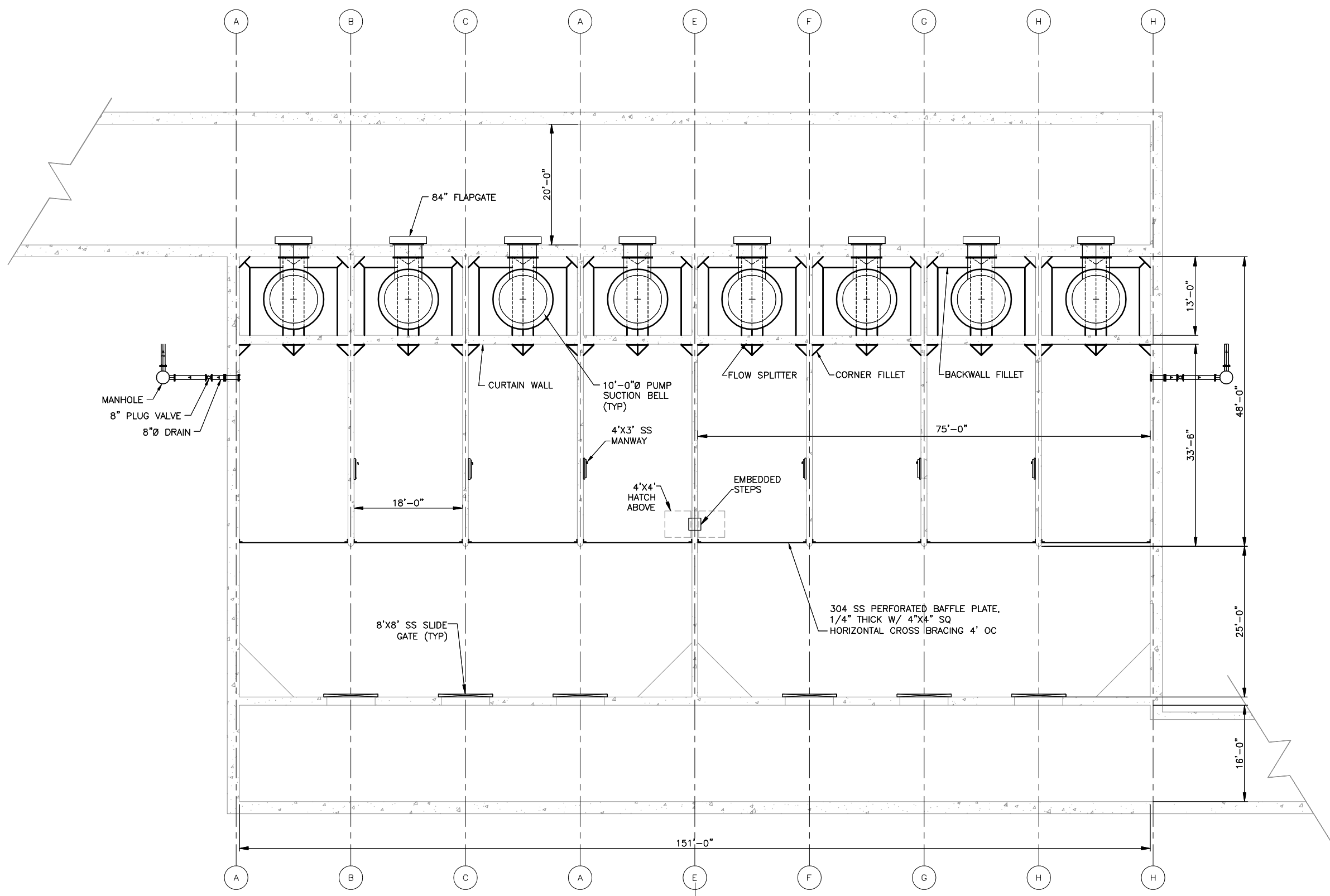
Main Stem Stage II Synthetic Maximum Water
Surface Elevations

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Plate A-178

— 2-year - - - 5-year - + - 10-year ····· 20-year - · - · 50-year — 100-year - - - - 500-year

**APPENDIX C
LLPS Proposed Layout**



Rev.	Description	Appr.	Date

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 Checked by: XX
 Drawn by: MB
 Date: 1/2008

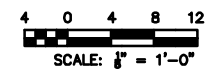
Correct: ANTHONY BOUCHARD
 Approved: MWRD Assistant Chief Engineer

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 ULTRAVIOLET DISINFECTION FACILITIES

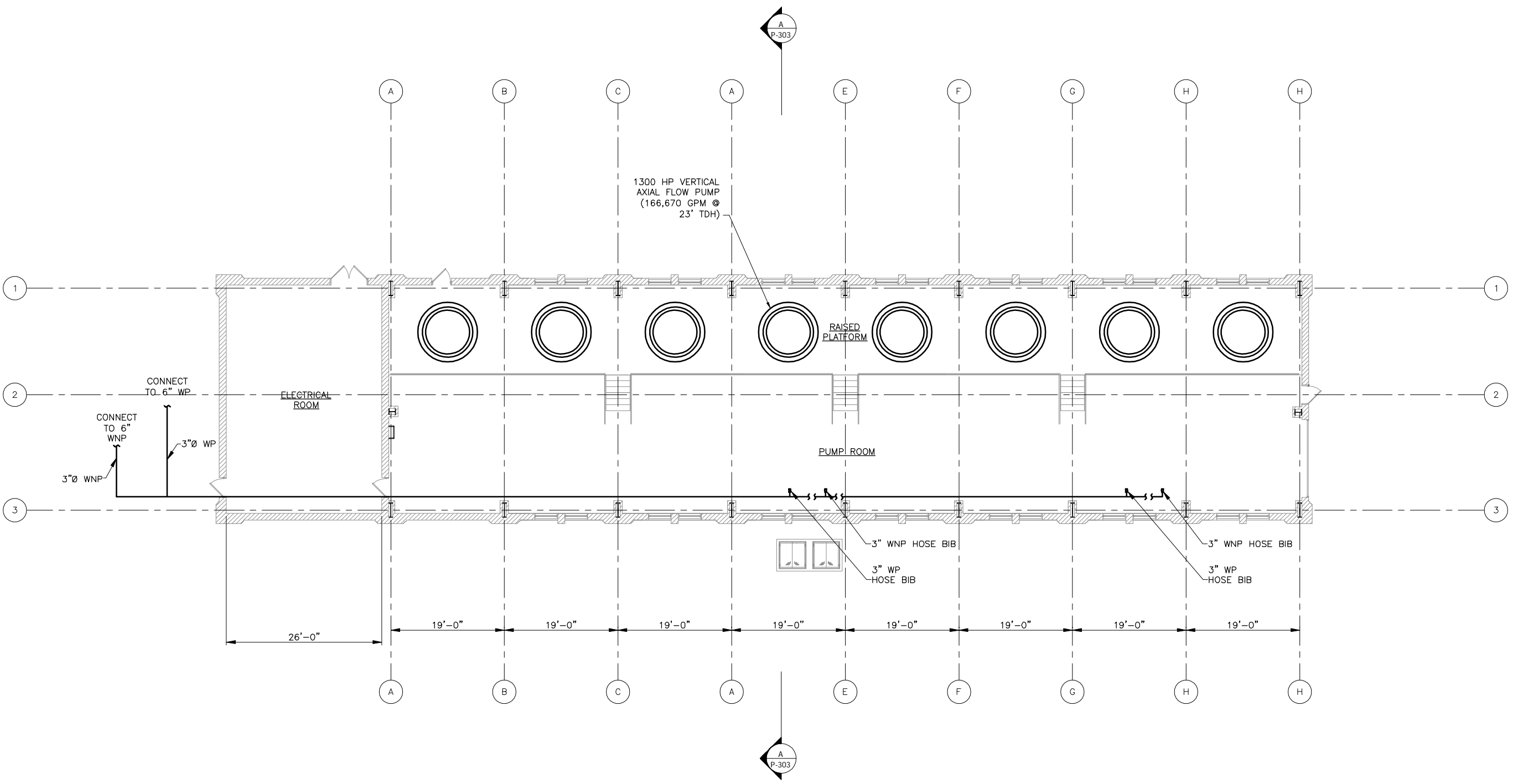
**LOW LIFT PUMP STATION
 LOWER LEVEL PLAN**

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P-301
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 MWRD Assistant Chief Engineer

Drawn by: MB
 Reviewed by: EPC
 Date: 1/2008

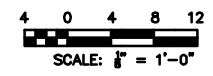
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**LOW LIFT PUMP STATION
 UPPER LEVEL PLAN**

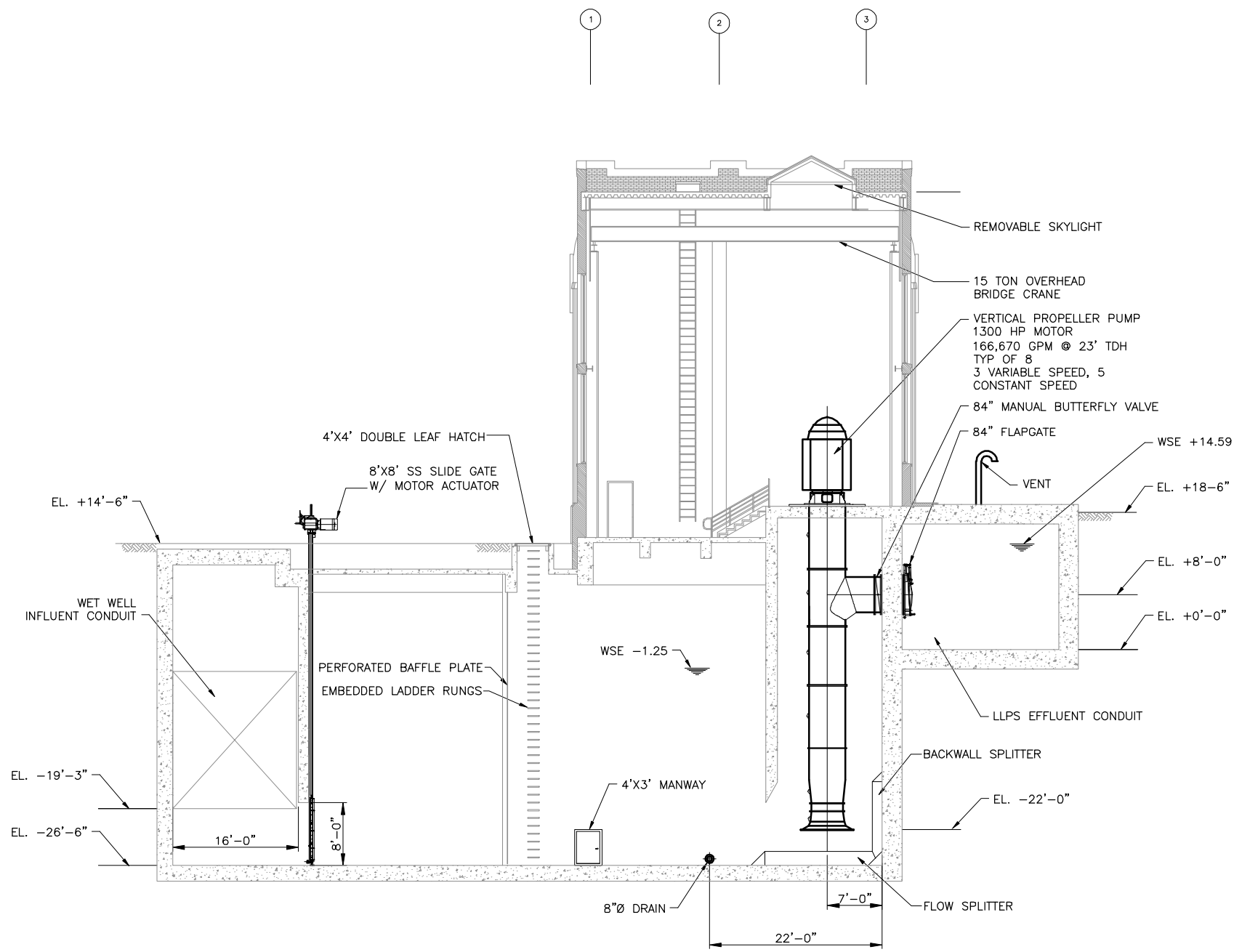
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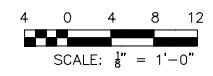
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